

Temperature effect on optical filter based on fiber-optic resonator using polarization and birefringence effects in the resonator loop

Abstract

In this paper an analysis of optical filter based on fiber-optic ring resonator using polarization and birefringence effects in the resonator loop is presented. The temperature variations, which affect the refractive index and radius of the ring, would cause a change in the filter response. The simulation results show that the resonant wavelengths would shift toward longer wavelengths and output intensity changes with increasing temperature. It is shown that for every 10 deg C change in temperature, would cause the resonance wavelength to increase by 0.1 μ m.

Keywords: optical filter, tunability, fiber-optic ring resonator, thermo-optic tuning, wavelength, refractive index, resonator loop, Sagnac ring, fiber optic gratings, polarizing sensors, biosensors, dispersion compensating devices

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Faramarz E Seraji, Saeede Gasemzade

Department of Communication Technology, Iran Telecom Research Center, Iran

Correspondence: Faramarz E Seraji, Faculty member Optical Communication Group, Department of Communication Technology, Iran Telecom Research Center, Tehran, Iran, Tel +98-21-84977723, Email feseraji@itrc.ac.ir

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Abbreviations: FORR, fiber-optic ring resonator; PR, polarization rotator

Introduction

Optical filters that are used today in fiber optic systems are designed based on various methods, such as fiber-optic ring resonator (FORR), Sagnac ring, fiber optic gratings, the use of arrayed waveguide gratings, or the use of dielectric thin-film interference structures and several other approaches. The tuning of these optical filters is also one of the key elements that should be taken into consideration, especially in WDM/DWDM optical communication systems, with channel spacing of less than 50 GHz. In this paper, the filter, which has been analyzed, is constructed on an FORR, with a resonance loop made up with a birefringent fiber.¹ Today, FORRs are used for various applications such as polarizing sensors, biosensors, dispersion compensating devices, optical switches, and other applications used in optical communication systems such as biosensors,² optical switching,³ add/drop multiplexers,⁴ micro disk laser resonators,⁵ simultaneous measurement of refractive index and temperature,⁶ optical Bistability,⁷ tunable optical filters,^{1,8} and several other applications used in optical communication systems. The use of FORR for tunable optical filters is analyzed, where the resonance loop of the FORR was made of photonic crystal fibers.⁹

A fiber-optic ring resonator with a resonance loop made of a conventional single-mode optical fiber as a nano-scale sensor for measurement of physical quantities, such as pressure and temperature is proposed.¹⁰ Recently, performance analyses of FORR under steady¹¹ and dynamic¹² states are reported, where the resonator responses in terms of characteristic parameters, are investigated. In our previous method, a Sagnac loop was used in an FORR to tune an optical filter which was based on variations of coupling coefficient and phase shift created by Sagnac rotation, and the fiber birefringence and propagating light polarization in the FORR. In this paper, we now want to study the effect of temperature variations on the filtering¹ and analyze its tunability at different conditions.

Theoretical foundations

In an FORR, any change that occurs on the structure and parameter of the loop, such as a change in loop radius and effective refractive index, makes the wavelength of the resonator change. One of the most important factors that change the radius of the FORR loop and the effective refractive index of the fiber is the temperature variations of the environment. Of course, the parameter that is more affected by the temperature changes is the effective refractive index of the fiber used in the FORR loop. The change in the wavelength of the FORR due to changes in the effective refractive index is given by the following equation:¹³

$$\frac{\Delta\lambda}{\lambda_0} = \left| \frac{\Delta n_{\text{eff}}}{n_{\text{group}}} \right| \quad (1)$$

To justify the above relation, we consider an optical fiber with a certain cross-section with propagation constant β . We assume that this optical fiber carries a wave with frequency ω under the influence of an external factor such as the variation of environmental temperature q .

When we examine the output of the filter, two degrees of freedom (q, ω) must be considered. The first one q is a minor change, then as a result, the propagation constant β changes as much as $\delta\beta_q$ and the resonance frequency is no longer ω . To revert the value of β to the original state, we change the frequency to reach the resonance condition, followed by a change $\delta\beta_\omega$ in β . The newly obtained frequency is considered to be tuned frequency. So, in general we have:

$$\beta \rightarrow \beta + \delta\beta_q \rightarrow \beta = \beta + \delta\beta_q + \delta\beta_\omega.$$

As a result, we have: $\delta\beta_q + \delta\beta_\omega = 0$. So, with the placement of the parameters, we have:

$$-\frac{\omega}{c} \frac{\partial n_{\text{eff}}}{\partial q} \Delta q + \frac{n_g}{c} \Delta \omega = 0 \quad (2)$$

If this external factor ΔT is due to temperature changes ΔT , we will have:

$$\frac{\Delta\omega}{\omega} = \frac{\Delta\lambda}{\lambda} = \frac{1}{n_g} \frac{\partial n_{\text{eff}}}{\partial T} \Delta T, \quad \text{for } \Delta\omega \ll \omega \quad (3)$$

Since the refractive index of the core differs from that of the fiber cladding, Eq. 3 changes as follows:

$$\frac{\Delta\lambda}{\Delta T} = \left| \frac{\lambda}{n_g} \left(\frac{\partial n_{\text{eff}}}{\partial n_{\text{co}}} \frac{\partial n_{\text{co}}}{\partial T} + \frac{\partial n_{\text{eff}}}{\partial n_{\text{cl}}} \frac{\partial n_{\text{cl}}}{\partial T} \right) \right| \quad (4)$$

where the terms $(\lambda / n_g)(\partial n_{\text{eff}} / \partial n_{\text{co}})$ and $(\lambda / n_g)(\partial n_{\text{eff}} / \partial n_{\text{cl}})$

are weighted coefficients that determine the amount of power in the corresponding region. These coefficients are calculated for each of the desired region as follows:

$$\Gamma = \frac{n_g}{n_A} \frac{\iint \epsilon |E|^2 dx dy}{\iint \epsilon |E|^2 dx dy} \quad (5)$$

where ϵ denotes the dielectric coefficient of the environment, n_A represents the group refractive index, and n_A is the refractive index of the region where the light wave penetrates. As a result, the refractive index of the core and the cladding regions change with respect to relative temperature variations as follows:

$$\begin{aligned} \Delta n_{\text{co}} &= \Gamma_{\text{co}} \left(n_{\text{co}} + \frac{dn_{\text{co}}}{dT} (T - T_0) \right) \\ \Delta n_{\text{cl}} &= \Gamma_{\text{cl}} \left(n_{\text{cl}} + \frac{dn_{\text{cl}}}{dT} (T - T_0) \right) \end{aligned} \quad (6)$$

where Γ_{co} , Γ_{cl} , and n_{co} , n_{cl} , respectively, are weighted coefficients and refractive indices of the core and cladding, and dn_{co} / dT and dn_{cl} / dT are corresponding thermo-optical coefficients. Different methods are used to calculate the thermo-optical coefficient of the fiber, among which interference is one of these methods.¹⁴ If we assume that fiber cladding is made of only pure silica and the fiber core is made with 15% GeO_2 mole combined with SiO_2 , the amount of thermo-optical coefficient will be 1.24 and 1.06, respectively. The schematic diagram of the fiber optic ring resonator is shown in Figure 1, where the incoming light wave enters the optical coupler with a definite polarization. By twisting the fiber on the xy -plane by the polarization rotator (PR) placed

$$\Delta\varphi = \sqrt{\varphi_c^2 + \left(\frac{\varphi_1}{2} \right)^2} \quad (7)$$

The x and y components of the normalized electrical fields just after PR are calculated as follows:

$$\begin{aligned} \frac{E_{tx}}{E_{in}} &= \frac{N_x}{D_x} \\ \frac{E_{ty}}{E_{in}} &= \frac{N_y}{D_y} \end{aligned} \quad (8)$$

where for parameters N_x , D_x , N_y , and D_y , respectively, we can write:

$$\begin{aligned} N_x &= - \left[1 + i\sqrt{\alpha k} e^{-i\omega\tau} \left(\cos \Delta\varphi - i \frac{\varphi_1}{2} \frac{\sin \Delta\varphi}{\Delta\varphi} \right) \right] \\ &\quad \left(\frac{E_{ty}}{E_{in}} \right) + i\alpha\sqrt{k(1-k)} e^{-2i\omega\tau} \left(\varphi_c \frac{\sin \Delta\varphi}{\Delta\varphi} \right)^2 \end{aligned} \quad (9)$$

$$D_x = i\sqrt{\alpha k} e^{-i\omega\tau} \varphi_c \frac{\sin \Delta\varphi}{\Delta\varphi} \quad (10)$$

$$\begin{aligned} N_y &= \left[\frac{\varphi_1 \varphi_c}{2} \left(\frac{\sin \Delta\varphi}{\Delta\varphi} \right)^2 \right] \times \\ &\quad \left[e^{-i\omega\tau} \sqrt{\alpha} \left(\sqrt{k} + \sqrt{1-k} \left(\frac{\varphi_c \sin \Delta\varphi}{\Delta\varphi} \right) \right) \right] \\ &\quad \left[-\alpha\sqrt{k(1-k)} e^{-2i\omega\tau} \right] \end{aligned} \quad (11)$$

$$\begin{aligned} D_y &= 1 + 2i\sqrt{\alpha k} e^{-i\omega\tau} \cos \Delta\varphi \\ &\quad - \alpha k e^{-2i\omega\tau} \left[\cos^2 \Delta\varphi + \frac{\varphi_1^2}{4} \frac{\sin^2 \Delta\varphi}{\Delta\varphi^2} \right] \end{aligned} \quad (12)$$

In the above expressions, k and α , respectively, are the coupling coefficient of the optical coupler and fiber transmission coefficient in the loop of the FORR. These two normalized electric fields are obtained by passing through the loop at the output of the filter as follows:

$$\frac{E_{ox}}{E_{in}} = -i\sqrt{k} + \sqrt{1-k} \frac{E_{tx}}{E_{in}} \quad (13)$$

$$\frac{E_{oy}}{E_{in}} = \sqrt{1-k} \frac{E_{ty}}{E_{in}} \quad (14)$$

where $\tau = (\Delta n_{\text{eff}} / c)L$ denotes the time delay of the FORR with the loop length of L and relative refractive index difference between the core and the cladding of Δn_{eff} . The fiber length is also increased by temperature variations. The longitudinal thermal expansion coefficient of fiber is equal to $\frac{1}{L} \frac{dL}{dT} = 2 \times 10^{-6} / {}^\circ\text{C}$ that is experimentally measured.¹⁶ Now, we introduce the temperature effects in corresponding Eqs. (3) to (6) in the normalized filter outputs expressed by Eqs. (13) and (14). If we choose the radius of the resonator ring at 15 μm and assume that the fiber is twisted through an angle 45 deg., thus the normalized output of the filter for different temperatures is obtained, as shown in Figure 2. As shown in Figure 2, when temperature increases, the resonance wavelength of the filter moves toward longer wavelengths. In Figure 3 the displacement of the resonance wavelengths at various temperatures from 20 to 80°C is indicated by a step of 10 degrees. At about 65°C onwards, the resonance wavelength varies linearly with respect to temperature changes. As the temperature increases, the

output intensity considerably decreases. A temperature increase of 20 °C from 40 °C to 60°C, would cause normalized output intensity drop down from 1400 to about 260.

PR, polarization rotator

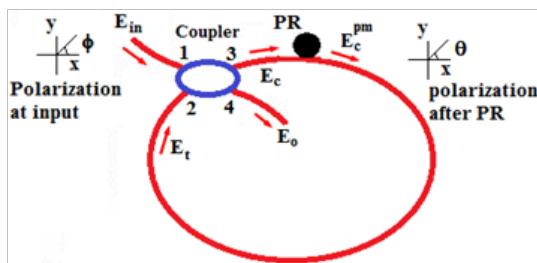


Figure 1 Schematic diagram of the Fiber optic resonator.¹

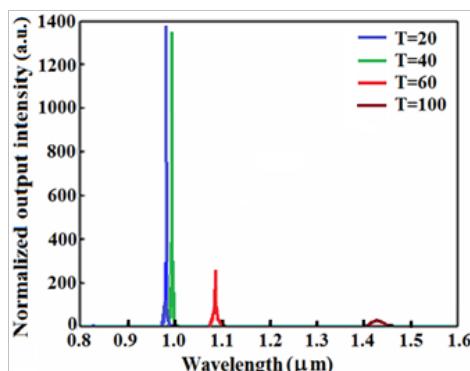


Figure 2 Normalized filter output for various temperatures from 20 °C to 100 °C.

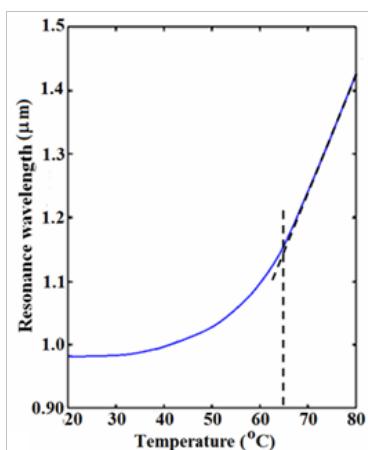


Figure 3 The effect of temperature on resonance wavelength of the filter.

Conclusion

In this paper, the optical filter behavior is analyzed with the effect of temperature variations using MATLAB software. In optical communication systems, temperature rise can be considered in two directions. In one way, whenever necessary, it could be used for tuning the filter. On the other hand, when the target is not tuning, the variations of the environmental temperature could drift the filter response which is undesired condition in practice. In the analysis, it is shown that for every 10 °C temperature change of the filter increases the resonance wavelength about 0.1 μm.

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Conflicts of interest

Authors declare there is no conflict of interest.

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