

Experimental studies on crushing behaviour of hexagonal composite tubes

Abstract

In this study, the effects of mandrel geometry on the crashworthiness performance of the fabric plain weave /epoxy hexagonal tubes are investigated. The energy absorption capacity of the tubes is investigated under uniaxial compression. An experimental, the crushing behaviour of composite hexagonally with aspect ratio 70 and different hexagonal angles ranging from 35° to 55° in 10° increment under axial crushing load were considered. The influence of tube side angles on the crashworthiness of (FPWEH) tubes is determined. Compressive testing indicates that the (H.70.45°) tube provides a specific absorbed energy of 10.7(kJ/kg), as well as average crushing load, which is the best value compared with other tubes. Furthermore, the failure modes noted as the progressive failure mode, Therefore, this study suggests that FPWEH tubes could be used in several structural applications, i.e. in automotive as energy absorbers and in civil infrastructure as poles.

Keywords: hexagonal tubes, energy absorption, crushing behaviour

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Introduction

Investigations of crushing energy absorption are important and are expected from the point of view of safety design of passenger vehicles. In order to reduce the damage to occupants in a collision, it's necessary to understand the crushing behaviour and to enhance the energy absorbing capability of tubular structures. In passenger vehicles, the ability to absorb impact energy and be survivable for the occupant is called the "crashworthiness" of the structure. This absorption of energy is through controlled failure mechanisms and modes that enable the maintenance of a gradual decay in the load profile.¹⁻³

The effect of the number of layers, type of the fiber, type of the matrix and fiber orientation angles were the common features which are usually evaluated for each structure by developing the load-displacement and energy absorption relation.⁴⁻⁶

Throughout this investigation, the energy absorption capability and failure modes in a hexagonal composite tube are carried out experimentally an axial crushing load.

Methodology

The wet hand lay-up technique was used to fabricate a Fabric plain weave /epoxy hexagonal shape composite tube. Woven Fabric plain weave was passed through a resin bath, causing resin impregnation. This was followed by the appliance of wet fibre to the solid wooden spindle to create the hexagonal composite. A layer of wax coated the outer surface of the mandrel in order to make it easier to extract the hexagonal from the mandrel. Two layers of Fabric plain weave /epoxy wrapped to get a thickness of approximately 2mm. The fabricated tubes were concerned at room temperature for 24hours to afford optimum stiffness and shrinkage.

Discussion

Hexagonal tube with aspect ratio (L/t=70 and β=35°)

Figure 1, shows a typical load-displacement curves and

deformation history for a hexagonal composite tube with an aspect ratio (L/t=70 and β=35°) subjected to the quasi-static compressive load. Linearity is evident during the pre-crushing stage as shown in Figure 1a & 1b. In this stage the tube resistance reaches first and highest peak $P_i=PH=14.3kN$ at a displacement of 4mm (0.05h) followed by a gradual decrease till it reaches the lowest load value $PL=0.6kN$ at displacement 24mm (0.32h). A rapid rise of the load carrying capacity was observed and reached its second peak value of 8.8kN at a displacement 33mm (0.44h). The splaying failure mode, then, occurred as result of local buckling as shown in Figure 1c. After that, the progressive folding is dominating the post -crushing stage as clearly illustrated in Figures 1d-1f.

Hexagonal tube with aspect ratio (L/t=70 and β=45°)

Figure 2 shows the load-displacement curves and deformation history of the hexagonal composite tube with an aspect ratio (L/t=70 and β=45°). Initially, the load increased linearly to its first peak $P_i=11.1kN$ at 1mm (0.009h) displacement. Hence, the tube resistance dropped gradually to 1.5kN at 10mm (0.09h) displacement. In this stage, the specimen is torn apart from the bottom end due to transverse crack and it is evident from (Figure 2(a)) (Figure 2(b)). The tube resistance was then recovered immediately to reach its second peak and highest peak $PH=13.3kN$ at 33mm (0.31h) displacement. Splaying failure mode with local buckling was initiated at the bottom end of the tube leading to a sudden drop of the load as shown in Figure 2c. A rapid rise of the load was observed following its sudden drop. Lastly, splaying failure mode dominated the post-crushing stage as clearly illustrated in Figures 2(d-f). The studies by Oshkovr et al.⁷ and Eshkoo et al.⁸ On silk/epoxy tubes showed that generally buckling (either local buckling or mid-length buckling) and hinge formation are the two main characteristics of woven silk/epoxy tubes, displaying a catastrophic failure.

Hexagonal tube with aspect ratio (L/t=70 and β=55°)

The load-displacement curves in Figure 3, shows crushing history of the hexagonal composite tube with an aspect ratio (L/t=70 and β=55°). Initially, the load rises almost linearly to its first peak

$P_i=14\text{kN}$ at 1mm ($0.009h$). High sudden drop was then noted due to transverse crack at the middle of the tube and after the sudden drop the load-displacement curve becomes almost stable about sustained a load value of 3.1kN for displacement between 7mm ($0.06h$) and 42mm ($0.4h$) displacement as shown in Figure 3a & b. Few tiny drops of load later appeared, evolving a transverse crack by splitting the tube into two segments as shown in Figure 3c & d. The tube resistance recovered immediately to reach its highest peak load value of 14.8kN at 87mm ($0.82h$) displacement. The tube finally collapsed as indicated in (Figure 3e) (Figure 3f).

A Crashworthiness parameters for hexagonal composite tube with aspect ratio ($L/t=70$) and various angles is summarized in Table 1.

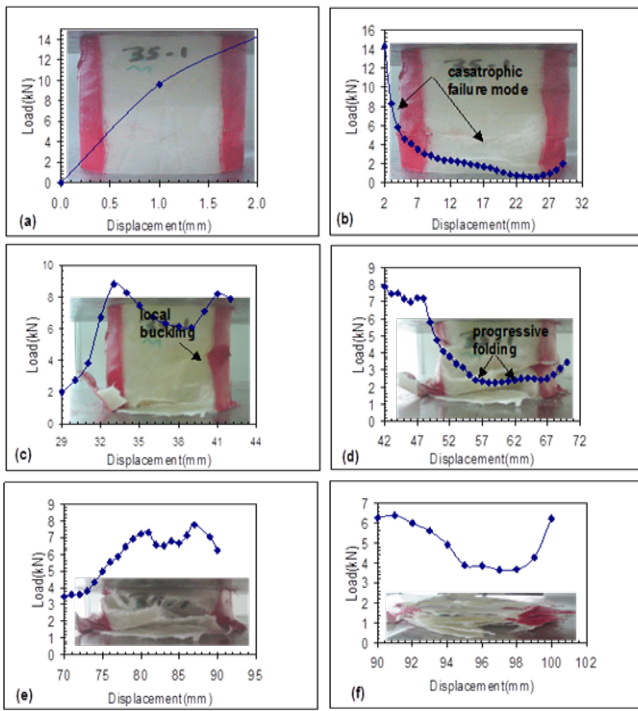


Figure 1 Typical load-displacement and crushing for (H.70.35°).

Table 1 Crashworthiness parameters for hexagonal composite tube with aspect ratio ($L/t=70$) and various angles

Specimens (ID)	P_i (kN)	E_s (kJ/kg)	P_{cr} (kN)
(H.70.35°)	11.5	6.96	11.5
(H.70.45°)	13.2	10.7	13.2
(H.70.55°)	8.5	8.6	8.5

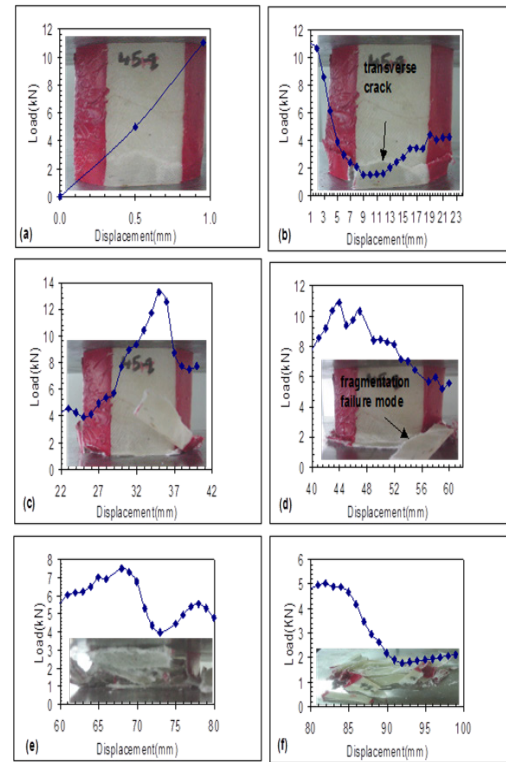


Figure 2 Typical load-displacement and crushing for (H.70.45°).

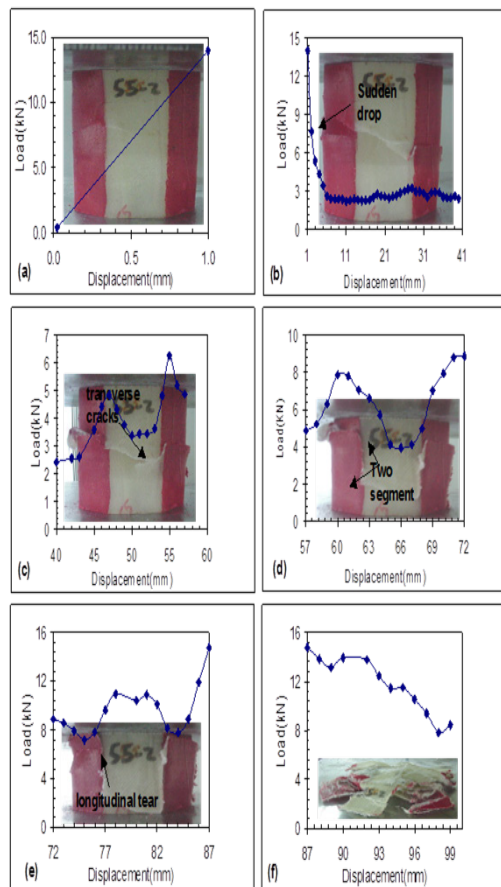


Figure 3 Typical load-displacement and crushing for (H.70.55°).

Conclusion

The main conclusions, which can be drawn, are:

- a. From the average crushing load value, it can be concluded that the average load increases as the hexagonal angle increases from 35°, the crush load becomes maximum at hexagonal angle 45°, the average crush load decreases as the hexagonal angle increases up to a hexagonal angle of 60°.
- b. The hexagonal tube with $\beta=45^\circ$ exhibited the highest energy absorption capability with value angle of 35° compared to the tubes with other tubes.
- c. It appears that, for these models of $L/t=70$, a transverse crack at any section of the tube at the pre-crushing stage leads to catastrophic failure mode followed by stable load-displacement behaviour.
- d. The failure of hexagonal tubes appeared as a progressive crushing type when subjected to compressive load.

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Conflict of interest

There is no conflict of interest.

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