

# Stochastic thermo-elastic stability analysis of laminated composite plates resting on elastic foundation under non-uniform temperature distribution

## Abstract

In this paper the stochastic thermo-elastic stability of laminated composite plates resting on elastic foundations under non-uniform temperature distribution is analyzed. The mathematical model is based on higher order shear deformation theory [HSDT] and von-Karman nonlinear kinematics is presented. A  $C^0$  nonlinear finite element method combined with direct iterative method in conjunction with mean centered first order Taylor series based perturbation technique is employed for the Eigen value problem in random environment to derive the second order statistics (mean and the standard deviation) of the thermal post buckling load under non-uniform temperature distribution. Typical numerical results for stacking sequence, no of plies, plate thickness ratios, amplitude ratios, aspect ratios, boundary conditions and temperature change are generated. Numerical results have been compared with available results in literatures and with independent Monte Carlo simulation [MCS].

**Keywords:** non uniform temperature distribution, thermal post buckling temperature, composite plates, system properties, elastic foundation, perturbation technique

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**Abbreviations:** MCS, monte carlo simulation; HSDT, higher order shear deformation theory; FEM, finite element method; SFEM, stochastic finite element method

## Introduction

Composite structures have inherent dispersion in system properties due to lack of strict quality control and the characteristics of the large parameters involved with the manufacturing and fabrication process. The transverse shear deformation effects are considerably pronounced in composite laminates and must be incorporated while studying the buckling and post-buckling behavior of laminates under in-plane thermally induced loading. Thermal buckling of geometrically nonlinear plate structures is one of the major design criteria for an efficient and optimal usage of materials and then buckling loads are of extremely inherent in the design and developments of high performance composite component for stability point of view. The variation in the system properties of the composite materials necessitates the inclusion of randomness of system properties in the analysis; otherwise predicted response may differ significantly rendering the structures unsafe. For reliable and safe design especially for sensitive engineering applications in thermal environments, accurate prediction of system behavior of composite structures in the present of uncertainties in the system properties favors a probabilistic analysis approach by modeling their properties as basic random variables.

A considerable amount of literature exists on the thermal buckling and post-buckling of laminated composite plates supported with and without elastic foundation subjected to non-uniform temperature with deterministic system properties. Notably among them are Chen et al.<sup>1</sup>

Shen,<sup>2</sup> Shen,<sup>3</sup> Shen and Zhu,<sup>4</sup> Shen and Lin,<sup>5</sup> Shen,<sup>6</sup> Shen.<sup>7</sup> The research based on the assumption of complete determinacy of the structural parameters, the inherent randomness in the structures is neglected. To well define the original problem for better understanding and characterization of actual behavior of laminated composite materials for sensitive applications and reliable design, it is obviously of prime importance that inherent randomness in the system parameters to be incorporated in the analysis. However, the analysis of the structures with randomness in system properties is not developed to the some extent. The deterministic analysis is not sufficient to predict system behavior due to various system uncertainties as it gives only mean response and misses the deviation caused by the system parameters.

A considerable amount of literature exists on the initial thermal buckling and post buckling of laminated composite plates with temperature dependent and temperature independent thermo-elastic material properties.<sup>8-14</sup>

However, the analysis of the structures with randomness in system properties is not developed to the same extent.<sup>15-18</sup> Nieuwenhof & Coyette<sup>19</sup> investigated sensitivity analysis to the random parameters such as material and shape parameters using SFEM and independent MCS. Stefanou & Papadarakakis,<sup>20</sup> Singh et al.<sup>21,22</sup> & Onkar et al.<sup>25,26</sup> have used a generalized layer wise stochastic finite element formulation for the buckling analysis of homogeneous and laminated plates with and without centrally loaded circular cutouts having random material properties using FOPT in conjunction with HSDT.<sup>25,27</sup>

The contribution of this paper is the investigation of HSDT based on  $C^0$  linear and nonlinear FEM in conjunction with mean centered FOPT, to compute the second order statistics of thermal post buckling temperature of laminated composite plates resting on

elastic foundation involving randomness in system parameters such as material properties, thermal expansion coefficients, foundation parameters and lamina plate thickness are modeled as independent random variables (RVs) assuming non-uniform tent like temperature and uniform constant temperature and a linearly varying transverse temperature distribution across the thickness under uni-axial and biaxial edge compression over entire surface of the plate. This approach is valid for system properties with small random dispersion compared with the mean values. The condition satisfies by most of the engineering materials and fortunately composites fall in these categories.

### Mathematical formulation

A rectangular laminated composite plate of length  $a$ , width  $b$ , and total thickness  $h$ , defined in  $(X, Y, Z)$  system with  $x$ - and  $y$  axes located in the middle plane and its origin placed at the corner of the plate with consisting of  $N$  orthotropic layers with the fiber orientation of  $(\theta_k)$ . Let  $(\bar{u}, \bar{v}, \bar{w})$  be the displacement parallel to the  $(X, Y, Z)$  respectively as shown in Figure 1. The thickness coordinate  $Z$  of the top and bottom surfaces of any  $k_{th}$  layer are denoted by  $Z_{(k-1)}$  and  $Z_{(k)}$  respectively. The fiber of the  $k_{th}$  layer is oriented with angle  $\theta_k$  to the  $X$ - axes. The plate is resting on elastic foundation excluding any separation during the process of deformation as shown in Figure 1. The load displacement relationship between the plate and the supporting foundation can be described by two-parameter model of the Pasternak-type as

$$P = K_1 w - K_2 \nabla^2 w \quad \text{with } P = K_1 w - K_2 \nabla^2 w. \tag{1}$$

Where,  $P$  is the foundation reaction per unit area, and  $\nabla$  is the Laplace differential operator,  $K_1$  and  $K_2$  are the Winkler and Pasternak Foundation stiffness,<sup>12</sup> respectively, and “ $w$ ” is the transverse displacement of the plate. This model is called Winkler type when  $K_2 = 0$ .

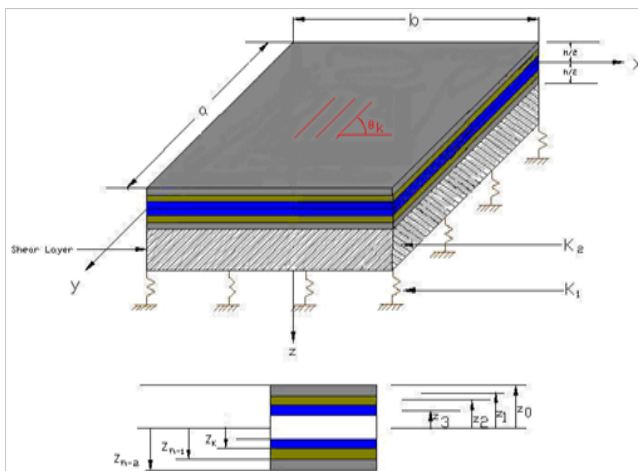


Figure 1 Geometry of laminated composite plate resting on elastic foundation.

### Displacement field model

In the present study the Reddy’s higher order shear deformation theory has been employed.<sup>16</sup> The difficulty and complexity associated with making a choice of  $C^1$  continuity is inherent generality and has led

to the development of nonconforming approaches. The displacement field model, after incorporating zero transverse shear stress conditions at the top and the bottom of the plate, is slightly modified, so that a  $C^0$  continuous element would be sufficient. The  $C^0$  continuity permits easy so parameters finite element formulation and consequently can be applied for non rectangular geometry is as well. In modified form, the derivatives of out-of-plane displacement are themselves considered as separate degree of freedom (DOFs). Thus five DOFs with  $C^1$  continuity are transformed into seven DOFs due to conformity with HSDT. In this change artificial constraints are imposed which can be enforced valiantly through the penalty approach, in ordered to satisfy the imposed.<sup>22,26</sup>

The displacement field along the  $x$ ,  $y$ , and  $z$  directions for an arbitrary composite laminated plate is now written as

$$\begin{aligned} \bar{u} &= u + f_1(z)\psi_x + f_2(z)\theta_x \\ \bar{v} &= v + f_1(z)\psi_y + f_2(z)\theta_y \\ \bar{w} &= w; \end{aligned} \tag{2}$$

Where  $u$ ,  $v$ , and  $w$  are corresponding displacements of a point on the mid plane.  $\psi_x$  and  $\theta_x$  are the rotations of normal to the mid plane about the  $y$ -axis and  $x$ -axis respectively. with  $\theta_x = w_{,x}$  and  $\theta_y = w_{,y}$

$$f_1(z) = C_1 z - C_2 z^3; \quad f_2(z) = -C_4 z^3 \quad \text{With}$$

$$C_1 = 1, C_2 = C_4 = 4h^2/3.$$

$$\{\bar{\epsilon}_T\} = \{\bar{\epsilon}^L\} + \{\bar{\epsilon}^{NL}\} - \{\bar{\epsilon}^T\}$$

The displacement vector for the modified  $C^0$  continuous model can be written as

$$\{\Lambda\} = [u \quad v \quad w \quad \theta_y \quad \theta_x \quad \psi_y \quad \psi_x]^T \tag{3}$$

With  $\theta_x = w_{,x}$  and  $\theta_y = w_{,y}$

Where, comma (,) denotes partial differentiation.

**Strain displacement relations:** The strain-displacements relations are obtained by using the small deformation theory with linear elasticity based on HSDT are expressed.<sup>10</sup>

**Stress-strain relation:** The constitutive relationship between stress resultants and corresponding strains of laminated composite plate accounting for thermal effect can be written as<sup>10,22,27</sup>

$$\{\sigma\}_k = [\bar{Q}]_k \{\epsilon\}_k \quad \text{or} \quad \begin{cases} \sigma_x \\ \sigma_y \\ \sigma_{xy} \\ \sigma_{yz} \\ \sigma_{xz} \end{cases}_k = \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} & 0 & 0 \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} & 0 & 0 \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} & 0 & 0 \\ 0 & 0 & 0 & \bar{Q}_{44} & \bar{Q}_{45} \\ 0 & 0 & 0 & \bar{Q}_{45} & \bar{Q}_{55} \end{bmatrix}_k \begin{cases} \epsilon_1 \\ \epsilon_2 \\ \epsilon_6 \\ \epsilon_4 \\ \epsilon_5 \end{cases}_k - \begin{cases} \lambda_1 \\ \lambda_2 \\ \lambda_{12} \\ 0 \\ 0 \end{cases}_k \delta_T \tag{4}$$

with

$$\lambda_1 = \bar{Q}_{11} \alpha_1 + \bar{Q}_{12} \alpha_2 + \bar{Q}_{16} \alpha_{12}; \quad \lambda_2 = \bar{Q}_{12} \alpha_1 + \bar{Q}_{22} \alpha_2 + \bar{Q}_{26} \alpha_{12}; \quad \lambda_{12} = \bar{Q}_{16} \alpha_1 + \bar{Q}_{26} \alpha_2 + \bar{Q}_{66} \alpha_{12}$$

where,  $[\bar{Q}]_k$ ,  $\{\sigma\}_k$  and  $\{\epsilon\}_k$  are transformed stiffness matrix,, stress and strain vectors of the  $k_{th}$  lamina, respectively and  $\alpha_x, \alpha_y, \alpha_{xy}$  are the thermal expansion coefficients along  $x$ ,  $y$ ,  $z$ ,

direction, respectively which can be obtained from the thermal coefficients in the longitudinal ( $\alpha_l$ ) and transverse ( $\alpha_t$ ) directions of the fibers using transformation matrix.  $T(X, Y, Z) = T_0 \left[ 1 + \frac{Z}{h} \right]$  is the uniform temperature [UT] and combined uniform temperature with linearly varying transverse temperature [TT] rise.  $\Delta T$  is the non-uniform tent-like temperature distribution. The non-uniform tent like temperature rise is assumed to be

$$\Delta T(X, Y, Z) = \begin{cases} T_0 + 2T_1 Y/b & 0 \leq Y \leq b/2 \\ T_0 + 2T_1(1-Y/b) & b/2 \leq Y \leq b \end{cases} \quad (5)$$

where  $T_0$  is the uniform temperature rise, and  $T_1$  is the temperature gradient, as shown in Figure 2. The constitutive relationship between stress resultants per unit length and mid-plane strains and curvatures can be written in matrix form.

$$\begin{Bmatrix} N_i \\ M_i \\ P_i \end{Bmatrix} = \begin{bmatrix} A_{ij} & B_{ij} & E_{ij} \\ B_{ij} & D_{ij} & F_{ij} \\ E_{ij} & F_{ij} & H_{ij} \end{bmatrix} \begin{Bmatrix} \varepsilon_j^0 \\ \kappa_j^0 \\ \kappa_j^2 \end{Bmatrix} - \begin{Bmatrix} N_i^T \\ M_i^T \\ P_i^T \end{Bmatrix} \quad (i, j=1, 2, 6) \quad (6)$$

$$\begin{Bmatrix} Q_2 \\ Q_1 \end{Bmatrix} = \begin{bmatrix} A_{4j} & D_{4j} \\ A_{5j} & D_{5j} \end{bmatrix} \begin{Bmatrix} \varepsilon_j^0 \\ \kappa_j^2 \end{Bmatrix}, \quad \begin{Bmatrix} R_2 \\ R_1 \end{Bmatrix} = \begin{bmatrix} D_{4j} & F_{4j} \\ D_{5j} & F_{5j} \end{bmatrix} \begin{Bmatrix} \varepsilon_j^0 \\ \kappa_j^2 \end{Bmatrix} \quad (j=4, 5) \quad (7)$$

Where  $A_{ij}, B_{ij}$ , etc., are the plate stiffness's defined in appendix. Thermal stress resultants

$$N_i^T = [N_{ix} \quad N_{iy} \quad N_{ixy}]^T, \quad M_i^T = [M_{ix} \quad M_{iy} \quad M_{ixy}]^T \quad \text{and}$$

$$P_i^T = [P_{ix} \quad P_{iy} \quad P_{ixy}]^T \quad \text{are calculated by}$$

$$[N_i^T, M_i^T, P_i^T] = \sum_{k=1}^N \int_{z_{k-1}}^{z_k} \begin{Bmatrix} \bar{Q}_{11}\alpha_x + \bar{Q}_{12}\alpha_y + \bar{Q}_{16}\alpha_{xy} \\ \bar{Q}_{12}\alpha_x + \bar{Q}_{22}\alpha_y + \bar{Q}_{26}\alpha_{xy} \\ \bar{Q}_{16}\alpha_x + \bar{Q}_{16}\alpha_y + \bar{Q}_{66}\alpha_{xy} \end{Bmatrix} (1, z, z^3) \Delta T dz \quad (8)$$

**Strain energy of the plate:** The potential energy ( $\Pi_1$ ) of the laminated composite plates can be expressed as

$$\Pi_1 = \frac{1}{2} \iint_R [N_x \varepsilon_{xx} + N_y \varepsilon_{yy} + N_{xy} \gamma_{xy} + Q_1 \gamma_{xz} + Q_2 \gamma_{yz}] dx dy \quad (9)$$

**Potential energy due to thermal stresses:** Due to uniform change in temperature, non-uniform tent like temperature distribution, pre-buckling stresses in the plate are generated. These stress resultants are the reason for the buckling. The potential energy due to the in plane thermal stress resultants is expressed as

$$\Pi_2 = \frac{1}{2} \int_A [N_x (w_{,x})^2 + N_y (w_{,y})^2 + 2N_{xy} (w_{,x})(w_{,y})] dA$$

$$(10) = \frac{1}{2} \int_A \begin{Bmatrix} w_{,x} \\ w_{,y} \end{Bmatrix}^T \begin{bmatrix} N_x & N_{xy} \\ N_{xy} & N_y \end{bmatrix} \begin{Bmatrix} w_{,x} \\ w_{,y} \end{Bmatrix} dA$$

Where,  $N_x$ ,  $N_y$  and  $N_{xy}$  are in plane applied thermal compressive stress resultants per unit length.

**Strain energy due to foundation:** The strain energy ( $\Pi$ ) due to elastic foundation having foundation layers can be written as:

$$\Pi_3 = \frac{1}{2} \int_A \left\{ K_1 (w_{,x})^2 + K_2 [(w_{,x})^2 + (w_{,y})^2] \right\} dA$$

$$(11) = \frac{1}{2} \int_A \begin{Bmatrix} w \\ w_{,x} \\ w_{,y} \end{Bmatrix}^T \begin{bmatrix} K_1 & 0 & 0 \\ 0 & K_2 & 0 \\ 0 & 0 & K_2 \end{bmatrix} \begin{Bmatrix} w \\ w_{,x} \\ w_{,y} \end{Bmatrix} dA$$

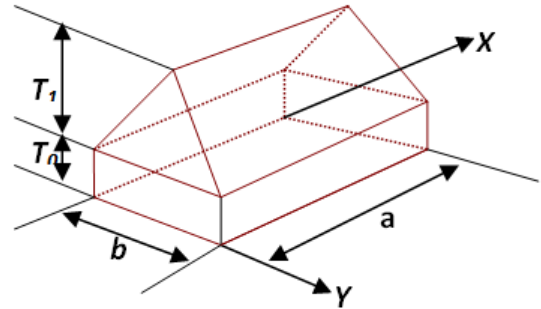


Figure 2 Geometry of non-uniform tent-like temperature distribution.

### Finite element model

**Strain Energy of the Plate Element:** In the present study a  $C^0$  nine-noded isoparametric finite element with 7 DOFs per node is employed. For this type of element, the displacement vector and the element geometry are expressed as

$$\{\Lambda\} = \sum_{i=1}^{NN} \varphi_i \{\Lambda\}_i; \quad x = \sum_{i=1}^{NN} \varphi_i x_i \quad \text{and} \quad y = \sum_{i=1}^{NN} \varphi_i y_i \quad (12)$$

Where  $i_{th}$  is the interpolation function for the  $i_{th}$  node,  $\{\Lambda\}$  is the vector of unknown displacements for the  $i_{th}$  node, NN is the number of nodes per element and  $x_i$  and  $y_i$  are Cartesian Coordinate of the  $i_{th}$  node.

Total potential energy which can be expressed as

$$\Pi_1 = \sum_{e=1}^{NE} \left[ \frac{1}{2} \{\Lambda(e)\}^T [K^{*(e)} + K_f^{(e)}] \{\Lambda(e)\} - \{\Lambda(e)\}^T [F_t^{(e)}] \right]$$

$$= \frac{1}{2} \{q\}^T [K + K_f] \{q\} - \{q\}^T [F^T] \quad (13)$$

With  $[K] = [K_b] + [K_s]$

Where global bending stiffness matrix  $[K_b]$ , shear stiffness matrix  $[K_s]$ , foundation stiffness matrix  $[K_f]$ , global displacement vector  $\{q\}$  and thermal load vector  $[F]$  are defined in the appendix.

### Thermal buckling analysis

Using finite element model Eq. (13), Eq. (11) after summing over the entire element can be written as

$$\Pi_2 = \sum_{e=1}^{NE} \Pi_2^{(e)}$$

$$= \frac{1}{2} \sum_{e=1}^{NE} \{\Lambda\}^T(e) \lambda [K_g]^{(e)} \{\Lambda\}^{(e)} dA$$

$$= \frac{1}{2} \lambda \{q\}^T [K_g] \{q\} \quad (14)$$

where,  $\lambda$  and  $[K_g]$  are defined as the thermal buckling load parameters and the global geometric stiffness matrix, respectively.

### Foundation analysis

Using finite element model

$$\Pi_3 = \sum_{e=1}^{NE} (\Pi_3^{(e)}) = \frac{1}{2} \int_A \{q^{(e)}\}^T [K_f]^{(e)} \{q^{(e)}\} \quad (15)$$

Where,  $[K_f]^{(e)}$  are the elemental linear foundation stiffness matrixes for the eth element.

Adopting Gauss quadrature integration numerical rule, the element linear and non-linear stiffness matrices, foundation stiffness matrix and geometric stiffness matrix respectively can be obtained by transforming expression in x, y coordinate system to natural coordinate system  $\xi, \eta$ .

### Governing equations

The governing equation for thermal buckling of laminated composite plate can be derived using Variational principle, which is generalization of the principle of virtual displacement. For the prebuckling analysis, the first variation of total potential energy ( $\Pi$ ) must be zero. By using Eq. 13 and Eq. 15

$$[K_l + K_{nl}\{q\}]\{q\} = [F^T] \quad (16)$$

Eq.16. can be rewritten as

$$[K]\{q\} = \lambda [K_g]\{q\}$$

$$\text{Where } [K] = [K_l + K_{nl}\{q\}]$$

For the critical buckling state corresponding to the neutral equilibrium condition, the second variation of total potential energy ( $\Pi = \Pi_1 + \Pi_2 + \Pi_3$ ) must be zero. Following this conditions, ones obtains as standard eigenvalue problem

$$[K + K_f] + \lambda [K_g]\{q\} = 0 \quad (17)$$

The stiffness matrix  $[K]$ , foundation stiffness matrix  $[K_f]$  and geometric stiffness matrix  $[K_g]$  are random in nature, being dependent on the system geometric and thermo-elastic properties. Therefore the eigenvalues and eigenvectors also become random. The (Eq. 17) can be solved with the help probabilistic FEM in conjunction with perturbation technique or Monte Carlo simulation (MCS) to compute the mean and variance of the thermal post buckling load.

### Solution technique: random thermal post buckling problem

Direct iterative method in conjunction with perturbation technique

#### Steps for the direct iterative technique

The nonlinear eigenvalue problem as given in (eq. 15), is solved by employing a direct iterative method in conjunction with the mean

centered first order perturbation technique assuming that the random changes in eigenvector during iterations does not affect the nonlinear stiffness matrices with the following steps.

By setting amplitude to zero, the random linear eigen value problem  $[K_l]\{q\} = \lambda [K_g]$  is obtained from the (Eq. 15), by assuming that the system vibrates in its principal mode. Then the random linear eigenvalue problem is broken up into zeroth and first order equations using perturbation technique by neglecting higher order equations. The zeroth order linear eigenvalue problem is solved by normal Eigen solution procedure to obtain the linear critical load parameters  $\lambda$  and the linear Eigen vector  $\{q_l\}$ . The first order perturbation equation is used to obtain the standard deviation of the thermal post buckling which is presented in next sub-section 6. 2. of perturbation technique.

- a. For a specified maximum deflection  $C$  at a center of the plate, the linear normalized eigenvector is scaled up by  $C$  times, so that resultant vector will have a displacement  $C$  at the maximum deflection point.

Using the scale-up eigenvector, the nonlinear terms in the stiffness matrix  $[K]$  can be obtained. The problem may now be treated as linear eigenvalue problem with a new updated stiffness matrix. The random eigenvalue problem can again be broken up into zeroth and first order equation using perturbation technique. The deterministic zeroth order can be used to obtain nonlinear critical load  $\lambda_{nl}$  and eigenvector  $\{q_{nl}\}$  and the random first order equations can be used to obtain the standard deviation (SD) of the Eigen solutions using the first order perturbation technique as presented in the next section.

Steps (ii)-(iii) are repeated by replacing  $\{q_l\}$  by  $\{q_{nl}\}$  in the step (ii) to obtain the converged mean and standard deviation of the nonlinear critical buckling load  $\lambda_{nl}$  to a prescribed accuracy ( $\approx 10^{-3}$ )

Steps (i) to (iv) are repeated for various value of  $C$ .

### Solution technique: perturbation technique

In the present analysis, the lamina material properties, thermal expansion coefficients and the geometric properties are treated as independent random variables (RVs). In general, without any loss of generality any arbitrary random variable can be represented as the sum of its mean and zero mean random part, denoted by superscripts 'd' and 'r', respectively.<sup>21</sup>

$$K = K^d + K^r, K_g = K_g^d + K_g^r, \lambda_i = \lambda_i^d + \lambda_i^r, q_i = q_i^d + q_i^r \quad (18)$$

Taylor's series keeping the first order terms and neglecting the second and higher order terms, collecting same order of the magnitude term, one obtains as<sup>37</sup>

Zeroth order:

$$[K^d]\{q_i^d\} = \lambda_i^d [K_g^d]\{q_i^d\} \quad (19)$$

First order:

$$[K^d]\{q_i^r\} + [K^r]\{q_i^d\} = \lambda_i^d [K_g^r]\{q_i^d\} + \lambda_i^d [K_g^d]\{q_i^r\} + \lambda_i^r [K_g^d]\{q_i^d\} \quad (20)$$

Eq. 19 is the deterministic equation relating to the mean eigenvalues and corresponding mean eigenvectors, which can be determined by conventional eigensolution procedures (eq. 20) is

the random equation, defining the stochastic nature of the thermal buckling which cannot be solved using conventional method. For this a further analysis is required.

$$\{q_i^d\}^T [K_g^d] \{q_i^d\} = \delta_{ij} \quad (21)$$

$$\{q_i^d\}^T [K^d] \{q_i^d\} = \delta_{ij} \lambda_i^d, (i, j) = 1, 2, \dots, p \quad (22)$$

Where  $\delta_{ij}$  is the Kronecker delta.

The eigenvectors, which meet orthogonality, conditions after being properly, normalized form a complete orthonormal set and any vector in the space can be expressed as their linear combination of these eigenvectors. Hence, the  $i^{\text{th}}$  random part of the eigenvectors can be expressed as

$$\{q_i^r\} = \sum_{j=1}^p C_{ij}^r \{q_j^d\}, C_{ii}^r = 0, C_{ii}^r = 0, i=1, 2, \dots, p \quad (23)$$

Where  $C_{ij}^r$ 's are small random coefficients to be determined.

Substituting eq. 23 in eq. 20, premultiplying, the first by  $\{q_i^d\}^T$  and second by  $\{q_j^d\}^T (j \neq i)$ , respectively and making use of orthogonality (eq. 22), one obtains as

$$\lambda_i^r = \{q_i^d\}^T [K^r] \{q_i^d\} - \lambda_i^d \{q_i^d\}^T [K_g^r] \{q_i^d\} \quad (24)$$

$$C_{ij}^r = \frac{\{q_j^d\}^T [K^r] \{q_i^d\} - \lambda_i^d \{q_j^d\}^T [K_g^r] \{q_i^d\}}{(\lambda_i^d - \lambda_j^d)}, \quad (25)$$

Substituting eq. 25 into eq. 23, we obtain

$$\{q_i^r\} = \sum_{j=1}^p \{q_j^d\} \frac{\{q_j^d\}^T [K^r] \{q_i^d\} - \lambda_i^d \{q_j^d\}^T [K_g^r] \{q_i^d\}}{\lambda_i^d - \lambda_j^d}, \quad \mathcal{A} \quad (26)$$

For the present case  $\lambda, \{q\}, [K]$  and  $[K_g]$  are random because of random geometric and material properties. Let  $b_1^r, b_2^r, b_3^r, \dots, b_q^r$  denote random variables (system properties).

The FEM in conjunction with FOPT has been found to be accurate and efficient.<sup>31-33</sup> According to this method, the random variables are expressed by Taylor's series expansion. The expression only up to the first-order terms and neglecting the second- and higher-order terms

$$b_1 = E_{11}, b_2 = E_{22}, b_3 = G_{12}, b_4 = G_{13}, b_5 = G_{23}, b_6 = \nu_{12},$$

The following dimensionless thermal buckling temperature, foundation parameters and post buckling temperature have been used in this study.

$$T_{cr} = \lambda_{cr} T \alpha_o * 1000; k_1 = K_1 b / E_{22} h^3; k_2 = K_2 b^2 / E_{23} h^3; \text{ and}$$

$$T_{cr} = \lambda_{cr} T \alpha_o * 1000$$

where  $\lambda_{cr}, \alpha_o, T, k_1$  and  $k_2$  are the dimensional mean thermal buckling load, the initial thermal expansion coefficient and the initial guessed temperature, Dimensionless Winkler and Pasternak foundation parameters, and  $\lambda_{cr}, \alpha_o$  and  $T$ , are dimensionless mean thermal post buckling temperature, initial thermal expansion coefficient and the initial guessed dimensionless temperature (980

are

$$\lambda_i^r = \sum_{j=1}^p \lambda_{i,j}^d h_j^r; \{q_i^r\} = \sum_{j=1}^p \{q_{i,j}^d\} h_j^r; \quad (27)$$

$$[K^r] = \sum_{j=1}^p [K^d]_{,j} h_j^r; [K_g^r] = \sum_{j=1}^p [K_g^d]_{,j} h_j^r$$

Where  $(, j)$  denotes the partial differentiation with respect to  $b_j$ .

On substitution of eq. 27 into eq. 24, one obtain as

$$\lambda_{i,j}^d = \{q_i^d\}^T [K^d]_{,j} \{q_i^d\} - \lambda_i^d \{q_i^d\}^T [K_g^d]_{,j} \{q_i^d\} \quad (28)$$

The variance of the eigenvalues can now be expressed as<sup>21</sup>

$$Var(\lambda_i) = \sum_{j=1}^q \sum_{k=1}^q \lambda_{i,j}^d \lambda_{i,k}^d Cov(b_j^r, b_k^r) \quad (29)$$

Where  $Cov(b_j^r, b_k^r)$  is the covariance between  $b_j^r$  and  $b_k^r$ . The standard deviation (SD) is obtained by the square root of the variance.

## Numerical examples and discussion

In present work a program in mat lab has been developed to find out Second-order statistics of the thermal buckling and thermal post buckling temperature for laminated composite plates subjected to uniform temperature (U.T.) distribution and combined uniform temperature with linearly varying temperature along transverse direction (T. T) and non-uniform tent like temperature distribution with random system properties. A nine noded Lagrange isoparametric element with 63 DOFs per element for the present HSDT model has been used for discretizing the laminate and (5×5) mesh has been used throughout the study. The mean and standard deviation of the thermal buckling temperature are obtained considering the random material input variables, thermal expansion coefficients, foundation parameters and lamina plate thickness taking combined as well as separately as basic random variables (RVs) as stated earlier. However, the results are only presented taking SD/mean of the system property equal to 0.10 as the nature of the SD (Standard deviation) variation is linear and passing through the origin. However the obtained results revealed that the stochastic approach would be valid upto SD/mean=0.20.<sup>32</sup> Moreover, the presented results would be sufficient to extrapolate the results for other SD/mean value keeping in mind the limitation of the FOPT. The basic random variables such as  $E_1, E_2, G_{12}, G_{13}, G_{23}, \nu_{12}, \alpha_1, \alpha_2, k_1, k_2,$  and  $h$  are sequenced and defined as

$$b_7 = \alpha_1, b_8 = \alpha_2, b_9 = k_1, b_{10} = k_{10}, b_{11} = h$$

applied in x and y direction respectively. In the present study various combination of edge support conditions such as all edges simply support conditions (SSSS) (S1 and S2), Clamped conditions (CCCC) and simply support and clamped condition (CSCS) have been used for the analysis .

The following relative numerical values and relationship between the mean valves of the material properties and thermal expansion coefficients for graphite/epoxy composite have been used in the present investigation.

$$E_{11}^d = 5.0E_{22}^d, G_{12}^d = G_{13}^d = 0.6E_{22}^d, G_{23}^d = 0.5E_{22}^d, \nu_{12}^d = 0.25,$$

$$\alpha_1^d = \alpha_0^d, \alpha_2^d / \alpha_1^d = 2 * \alpha_o, \alpha_o^d = 1 * 10^{-6}, E_{22}^d = 1 * 10^5.$$

The plate geometry supported with elastic foundation used is characterized by various aspect ratios, side to thickness ratios, lamination scheme and number of layers.

The plate geometry used is characterized by aspect ratios ( $a/b$ ) = 1 and 2, side to thickness ratios ( $a/h$ ) = 20, 30, 40, 50, 60, 80 and 100. The only exception is the Poisson's ratio, which can reasonably be assumed as constant deterministic due to weakly dependency on temperature change. The relation among elastic constants for the plate having all plies of equal thickness and temperature dependent material properties is given as.<sup>12,13</sup> For the temperature independent material properties (TID)  $E_{111}, E_{221}, G_{121}, G_{131}, G_{231}, \alpha_{111}$  and  $\alpha_{221}$  quantities are equal to zero. The material properties for non-uniform tent like and parabolic distribution are used as:

## Validation study

### Validation for mean buckling temperature for composite plate

The dimensionless mean thermal post buckling loads ( $T_{crnl}$ ) of angle-ply  $(\pm 45^0)_{2T}$  square laminated composite plate, temperature

$$E_{110} / E_{220} = 40, G_{120} / E_{220} = G_{130} / E_{220} = 0.2, \nu_{12} = 0.25, \alpha_{110} = \alpha_{220} = 1.0 \times 10^{-6} / ^0 C, E_{221} = G_{121} = G_{131} = G_{231} = \alpha_{111} = \alpha_{221} = 0$$

with simple support SSSS (S1) boundary conditions are compared for validation in Figure 5. It is observed the present results are good in agreements and validated with semi analytical approach by Shen.<sup>12</sup>

The present theoretical model is validated by comparing the mean dimensionless results with those available in literature<sup>9</sup> (Figure 3). Compares the results obtained from present FEM with existing results for a two layer and four layer anti-symmetric  $[45^0 / -45^0]$  and  $[45^0 / -45^0]_{2T}$  square laminate, ( $a/h=20$ ), for all edges CCCC supported boundary condition respectively. The

$$E_{110} / E_{220} = 40, G_{120} / E_{220} = G_{130} / E_{220} = 0.2, \nu_{12} = 0.25, \alpha_{110} = \alpha_{220} = 1.0 \times 10^{-6} / ^0 C, \\ E_{221} = G_{121} = G_{131} = G_{231} = \alpha_{111} = \alpha_{221} = 0$$

The post buckling temperature results are compared in Figure 6 with<sup>9</sup> of FSDT results and<sup>13</sup> of HSDT results.

Thermal post buckling response of angle-ply  $(\pm 45^0)_{6T}$  square laminated composite thin plates with amplitude ratios

$$E_{110} / E_{220} = 40, G_{120} / E_{220} = G_{130} / E_{220} = 0.2, \nu_{12} = 0.25, \alpha_{110} = \alpha_{220} = 1.0 \times 10^{-6} / ^0 C, \\ E_{221} = G_{121} = G_{131} = G_{231} = \alpha_{111} = \alpha_{221} = 0.$$

The post buckling temperature results are compared in (Figure 7) with Shen<sup>13</sup> of HSDT results. To validate the present method, the results for thermal post buckling of a simply supported thin ( $b/h=20$ ) square plate under non-uniform loading and resting on two parameters elastic foundation are listed in Figure 8 and compared with these given by Shen.<sup>3</sup> Clearly results obtained from present HSDT approach are in good agreement with the solution obtained from Riser midline plate theory approach.

independent (TID) and temperature dependent (TD) material properties, without foundations ( $k_1=0, k_2=0$ ), subjected to uniform constant temperature rise (U.T), ( $T_{crl}$ )- linear solution, plate thickness ratio ( $a/h$ ) =30, amplitude ratios ( $W_{max} / h$ ) with simply supported (S2) boundary conditions are compared for validation in Figure 4 with the results of available literature given in Shen.<sup>8</sup> Clearly, it is seen that the present results are in good agreement. The difference of the two results is due to the HSDT employed in present result whereas semi analytical approach used by Shen.<sup>12</sup>

The dimensionless mean thermal post buckling load of angle-ply  $(\pm 45^0)_{6T}$  square laminated composite thin plate with temperature-dependent thermo material properties and subjected to uniform temperature rise. Amplitude ratio ( $W_{max} / h$ ), random input variables  $E_{111} (0.0, -0.5 \times 10^{-4}, -0.2 \times 10^{-3})$  where  $E_{111}$  is assumed to be function of temperature, plate thickness ratio ( $a/h$ ) =100. Material properties are

results obtained HSDT are excellent agreement with FSDT results of literature.<sup>9</sup>

Thermal post buckling response of angle-ply  $(\pm 45^0)_{6T}$  square laminated composite thin plates with amplitude ratios having temperature-dependent thermo-elastic properties and subjected to a uniform temperature rise with simple support SSSS (S1). Where  $E_{111}$  is assumed to be function of temperature and  $E_{111} = -0.5 \times 10^{-4}, -0.1 \times 10^{-3}$  and  $-0.2 \times 10^{-3}$  respectively,  $b/h=100$ , material properties are

having temperature-dependent thermo-elastic properties and subjected to a uniform temperature rise with simple support SSSS (S2). Where  $E_{111}$  is assumed to be function of temperature and  $E_{111} = -0.5 \times 10^{-4}, -0.1 \times 10^{-3}$  and  $-0.2 \times 10^{-3}$  respectively,  $b/h=100$ , material properties are

Figure 9 examines the thermal post buckling load of 4-ply anti-symmetric angle-ply  $(\pm 45^0)_{2T}$  laminated composite square plate under non-uniform temperature distribution,  $b/h=10$  with simply supported S2 boundary conditions and are compared with those of Shen<sup>4</sup> and Shen & Lin.<sup>5</sup> Clearly, the results obtained from the present method accord quite well with the existing ones.

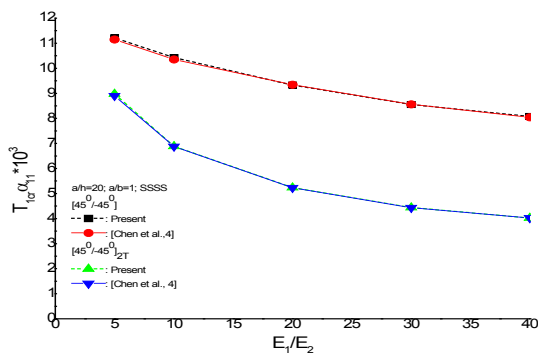


Figure 3 Validation study for analytical results.

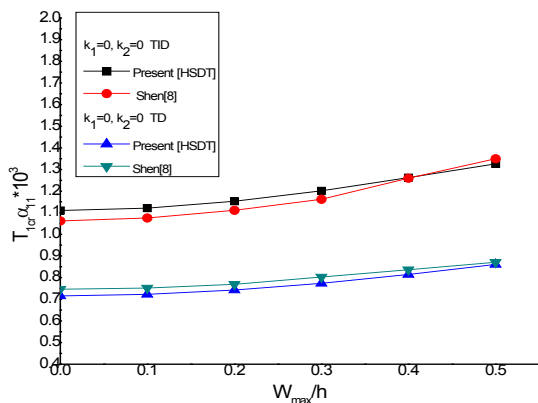


Figure 4 Validation study for analytical results.

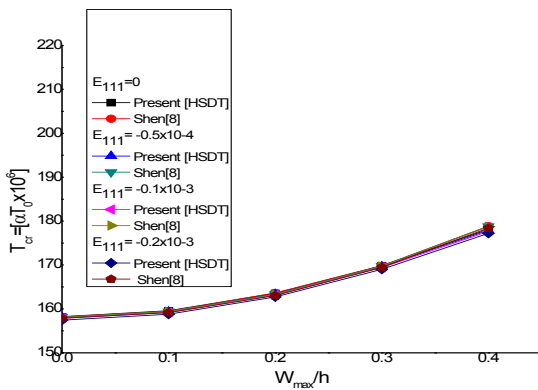


Figure 5 Validation study for analytical results.

### Validation study for random material and geometric properties

The present results of thermal buckling and post buckling load of laminated composite plates obtained from present FOPT approach have been compared and validated with an independent MCS approach.

### Validation result for random material and geometric properties (TID)

(Figure 10) (Figure 11) plot the normalized standard deviation, SD/mean (i.e. the ratio of the standard deviation (SD) to the mean value), of the thermal buckling load versus the SD/mean of the random material

constant and geometric parameter for an all simply supported cross-ply  $[0^0/90^0]$  and angle-ply  $[45^0/-45^0]$  square laminated composite plate subjected to non-uniform tent-like temperature distribution changing from 0 to 20% respectively. It is assumed that one of the material property (i.e.,  $E_{22}$ ) and lamina plate thickness  $h$  changing at a time keeping other as a deterministic, with their mean values. The dashed line is the present [FOPT] result that is obtained by using FOPT and the solid line is independent MCS approach. For the MCS approach, the samples are generated using Mat Lab to fit the desired mean and SD. The number of samples used for MCS approach is 10,000 for material properties and 12,000 for lamina plate thickness based on satisfactory convergence of the results. The normal distribution has been assumed for random number generations in MCS.

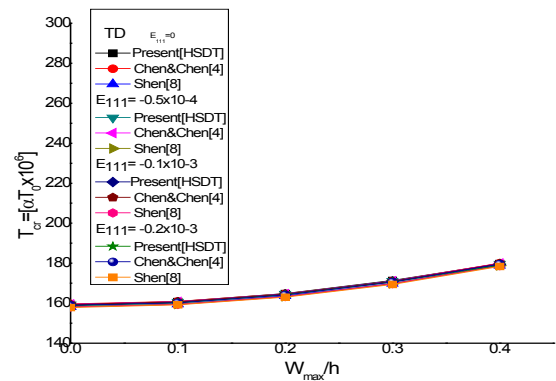


Figure 6 Validation study for analytical results.

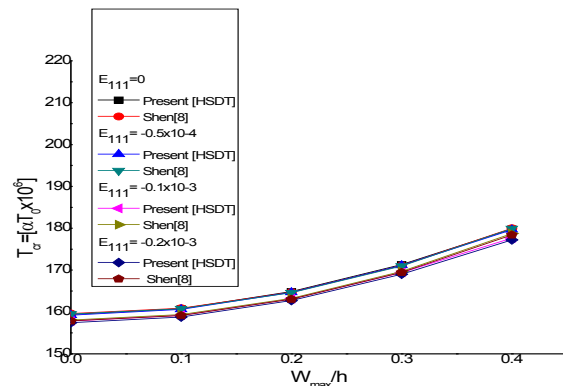


Figure 7 Validation study for analytical results.

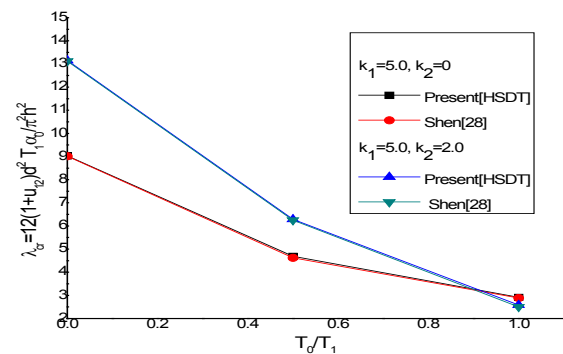


Figure 8 Validation study for analytical results.

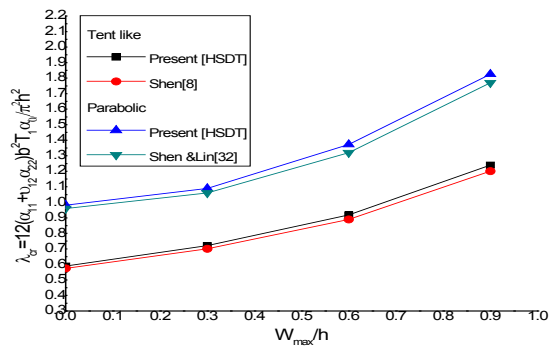


Figure 9 Validation study for analytical results.

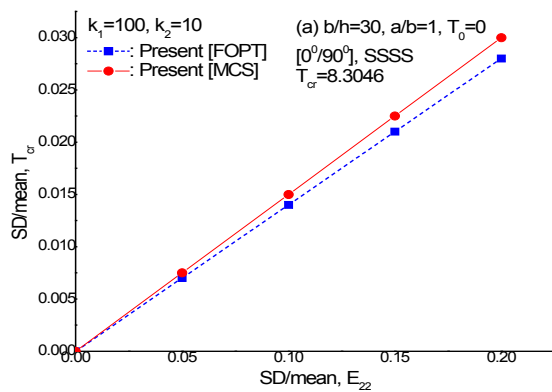


Figure 10 Validation of results the present FOPT approach from the independent MCS approach.

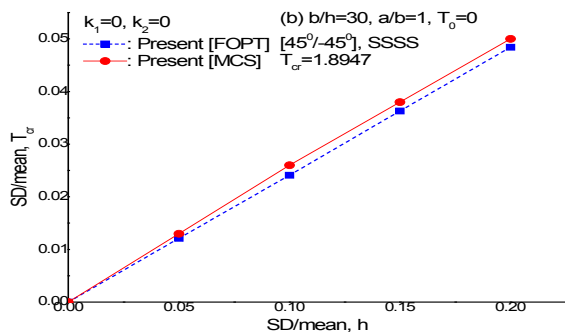


Figure 11 Validation of results the present FOPT approach from the independent MCS approach.

### Validation result for random material and geometric properties (TD)

(Figure 12) (Figure13) plots the normalized standard deviation, SD (i.e. the ratio of the standard deviation (SD) to the mean value), of thermal post buckling load versus the SD to the mean value of the random material property ( $E_{11}$ ) and geometric properties such as plate thickness ( $h$ ) for all simply supported (S2) angle-ply and cross-ply anti-symmetric  $[0^\circ/90^\circ]$  square laminated composite plate  $a/h=20$  with amplitude ratio ( $W_{max}/h=0.2$ ) and uniform temperature distribution changing from 0 to 20% subjected to biaxial compression with TD thermo-material properties. It is assumed that one of the material property (i.e.,  $E_{11}$ ) and geometric property (i.e.,  $h$ ) change at a time keeping others as deterministic, with their mean values of the material

and geometric properties. From the (Figure 12) (Figure 13) it is clear that, close correlation is achieved between two results subjected to TD thermo-material properties.

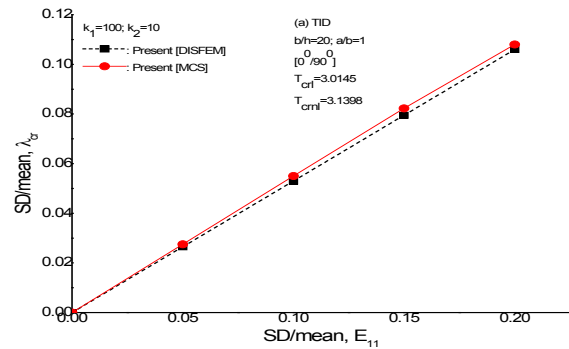


Figure 12 Validation of results the present DISFEM approach from the independent MCS approach.

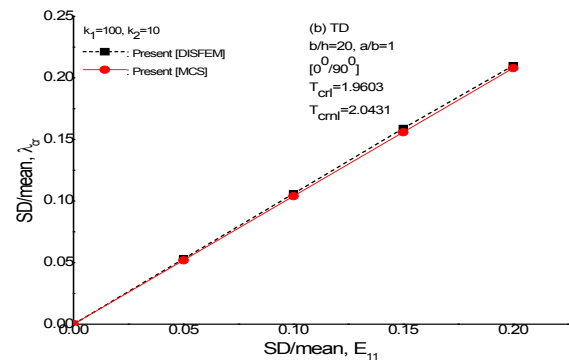


Figure 13 Validation of results the present DISFEM approach from the independent MCS approach.

## Numerical results: second order statistics of thermal buckling and post buckling temperature

### Parametric analysis of second order statistics (TD)

Table 1: It is observed that increase in amplitude ratio ( $W_{max}/h$ ) increases the mean thermal post buckling load and COV. Random input variable thickness ( $h$ ) effects are significant where as shear modulus  $G(12)$  effects are least for uniform temperature (U.T) as well as combined uniform with transverse temperature (T.T) distribution. However for (T.T) temperature distribution, individual random input variables  $E_{11}$ ,  $E_{22}$ ,  $G_{12}$  and  $h$  have fewer effects whereas the other random input variables have no effects compared to uniform temperature distribution.

Table 2: The thermal buckling temperature is most affected by random change in the  $E_{11}$  and  $h$  in the case of plate supported without foundation ( $k_1=0, k_2=0$ ) while  $k_1$  and  $h$  for Winkler elastic foundation ( $k_1=100, k_2=0$ ) and  $k_2$  and  $h$  for Pasternak elastic foundation ( $k_1=100, k_2=10$ ) respectively, and the least affected by  $\alpha_2$  in all the foundation cases. From the table it is clear that the dimensionless mean thermal buckling temperature increases when the plate supported with elastic foundation as the stiffness of the plate increases.

Table 3: It is expected that the thermal post buckling temperature increases as the amplitude ratio increases. It is observed that thermal



post buckling strength is more pronounced when the plate becomes relatively thick. The COV of the thermal buckling temperature increases as the plate thickness ratio increases for all random system parameters  $b_i$ ,  $\{i = (1, \dots, 8), (7, 8) \text{ and } (9)\}$  varying simultaneously or individual.

**Table 1** Effects of individual random variables [ $b_i$  ( $i = 1$  to  $9$ ) = 0.10], keeping others as deterministic with amplitude ratio  $(W_{max} / h)$  on the dimensionless mean  $(T_{crnl})$  in brackets and coefficient of variations  $(\lambda_{crnl})$  of thermal post buckling load of angle ply  $[\pm 450]_{3t}$  square laminated composite plates under combination of uniform and transverse temperature (t.t), uniform temperature (u.t) distribution., plate thickness ratio  $(a/h) = 30$  with simple support ssss (s2) boundary conditions. tcr1 = dimensionless linear mean thermal buckling load

$b_i$	$W_{max} / h$	(TD), COV, $\lambda_{crnl}$	
		(T.T)	(U.T)
		Mean $T_{crnl} = 80.8726$	Mean $T_{crnl} = 80.8726$
$E_{11} (i = 1)$	0.2	(0.8160) 0.0064	(0.8161) 0.0061
	0.4	(0.8917) 0.0073	(0.8918) 0.0063
	0.6	(0.9872) 0.0084	(0.9872) 0.0068
$E_{22} (i = 2)$	0.2	0.0135	0.0135
	0.4	0.0115	0.0117
	0.6	0.0086	0.0088
$G_{13} (i = 4)$	0.2	1.50e-04	1.32e-04
	0.4	2.27e-04	1.73e-04
	0.6	3.17e-04	2.30e-04
$G_{13} (i = 4)$	0.2	0.0059	0.0059
	0.4	0.0057	0.0057
	0.6	0.0057	0.0057
$G_{23} (i = 5)$	0.2	0.0024	0.0024
	0.4	0.0023	0.0023
	0.6	0.0023	0.0023
$V_{12} (i = 6)$	0.2	0.0815	0.0815
	0.4	0.0749	0.0749
	0.6	0.0682	0.0682
$\alpha_{11} (i = 7)$	0.2	0.079	0.079
	0.4	0.0723	0.0723
	0.6	0.0653	0.0653
$\alpha_{22} (i = 8)$	0.2	0.0017	0.0017
	0.4	0.0016	0.0016
	0.6	0.0014	0.0014
$h (i = 9)$	0.2	0.2183	0.2175
	0.4	0.2102	0.2094
	0.6	0.2031	0.2024

Table 4: For the fixed foundation parameters, the thermal buckling temperature increases as the plate thickness ratio decreases and vice versa for the case of dispersion. The thin plate ( $a/h = 20$ ) supported on Pasternak elastic foundation shows the highest dispersion with random change in all material properties and lamina plate thickness. However no definite trend is observed with random change in foundation parameters.

Table 5: It is observed that increase of amplitude ratio increases the mean thermal post buckling temperature in both (U.T) and (T.T) temperature distribution. The effects of aspect ratios decreases the mean thermal post buckling temperature and dispersion significantly increases. If lay-up is changed then for square plate the mean thermal post buckling temperature decreases and for rectangular plate increases. The COV is significantly increased by increase of aspect ratio. The difference in results of (U.T) and (T.T) temperature distribution is insignificant.

Table 6: For the fixed foundation parameters and number of layers, rectangular plate shows higher dispersion to random change in material properties plus thermal expansion coefficients and vice versa for random change in thermal expansion coefficients, foundation parameters and lamina plate thickness. For the same aspect ratio and foundation parameters, as the number of layer increases the dimensionless mean and dispersion increases for random change in all system properties.

Table 7: It is observed the increase of amplitude ratio increases the mean thermal post buckling temperature and decreases the dispersion for both (U.T) and (T.T) temperature distribution. Clamp support (CCCC) conditions significantly affect the thermal post buckling temperature and lowers the dispersions where as simple support conditions have least effects. It shows that for CCCC boundary conditions can withstand higher thermal post buckling temperature. On comparing uniform temperature and combined uniform with transverse temperature distribution the difference in parameters is very less.

Table 8: For the three cases of support conditions, the plate with CCCC boundary condition shows the highest thermal buckling temperature and its scattering, while the SSSS plate shows the least for the fixed foundation parameters considered. For the fixed support conditions, the thermal buckling temperature is greatest for plate resting on Pasternak elastic foundation, while least for plate without elastic foundation. From the table it can be seen that the scattering in the thermal buckling temperature is strongest to random change in all eight system parameters in the case of plates resting on Winkler elastic foundation with SSSS and CCCC support conditions, while strongest for plate without elastic foundation in case of CSCS support condition. The dispersion in the plates resting on Pasternak elastic foundation is highest with random change in foundation parameters and lamina plate thickness, while plate without foundation shows highest dispersion with the random change in thermal expansion coefficients.

Table 9: It is noticed that on rise in temperature the mean thermal post buckling temperature decreases for TID material properties, however the coefficient of variations for combination of input random variables and considering only thermal coefficients or geometric property plate thickness also decreases. For the TD material properties there is further decrease of expected mean thermal post buckling temperature while the COV for all input random variables increases

which is an important parameter when the rise of temperature is taken into consideration.

Table 10: For the TD material properties there is further decrease of expected mean thermal post buckling temperature while the COV for all input random variables increases which is an important parameter when the rise of temperature is taken into consideration.

Table 11: For the fixed foundation parameters, an anti-symmetric plate shows higher dispersion to random change in all system properties. However the mean thermal buckling temperature of symmetric cross-ply plate is higher than anti-symmetric cross-ply plate.

(Table 12) (Table 13): The effects of amplitude ratios increases the mean thermal post buckling temperature and decreases the COV in both uniaxial and biaxial compression with TD and TID thermo-material properties, however the effects are more dominant in uniaxial TID for mean thermal post buckling load and dispersion in biaxial TD compression respectively. Among individual random variation in material properties, thermal expansion coefficients and plate thickness

**Table 2** Effects of individual random input variables  $\{b_i, (i = 1 \text{ to } 11) = 0.10\}$  keeping other as deterministic at a time with various foundation stiffness parameters on the dimensionless mean and dispersion of thermal buckling temperature of anti-symmetric, angle-ply [450/-450/450/-450] square laminates with ssss boundary conditions subjected non-uniform tent like structures.

	$(k_1=0, k_2=0)$	$(k_1=100, k_2=0)$	$(k_1=100, k_2=10)$
<b>bi</b>	$MeanT_{crnl} = 17.9472$	$MeanT_{crnl} = 39.0972$	$MeanT_{crnl} = 80.8726$
	$COV, \lambda_{crnl}$	$COV, \lambda_{crnl}$	$COV, \lambda_{crnl}$
$E_{11} (i = 1)$	0.0697	0.032	0.0155
$E_{22} (i = 2)$	0.051	0.0234	0.0113
$G_{12} (i = 3)$	3.29E-04	1.54E-04	7.42E-05
$G_{13} (i = 4)$	0.0056	0.0026	0.0012
$G_{23} (i = 5)$	0.0046	0.0021	0.001
$V_{12} (i = 6)$	0.0142	0.0065	0.0031
$\alpha_{11} (i = 7)$	0.0011	5.20E-04	2.51E-04
$\alpha_{22} (i = 8)$	1.35E-04	6.19E-05	2.99E-05
$k_1 (i = 9)$	0	0.0541	0.0261
$k_2 (i = 10)$	0	0	0.0517
$h (i = 11)$	0.0488	0.1332	0.213

the COV is significant decreases for plate thickness in uniaxial as well as in biaxial for TD and TID material properties. As a matter of facts the COV for temperature dependent thermo material properties is of significant nature.

Table 14: It can be seen that the laminated plate under non-uniform tent-like temperature distribution has higher initial buckling load and post buckling load than non-uniform parabolic temperature distribution for the same thermal load ratio. It can also be seen that thermal post buckling strength under non-uniform tent like temperature distribution is more pronounced when the plate becomes heavily loaded thermal load as compared to parabolic temperature distribution. The dispersion of thermal post buckling temperature are same for both of the non-uniform tent-like and parabolic temperature distribution are almost same for all random system parameters  $b_i, \{i = (1, \dots, 8) \text{ and } (7, 8)\}$  varying simultaneously. However, dispersion of thermal post buckling temperature of the plate subjected to non-uniform tent-like distribution is higher than parabolic temperature distribution having random lamina properties  $b_i, \{i = (9)\}$ .

**Table 3** The comparison of variation of plate thickness ratios ( $a/h$ ) with amplitude ratios  $(W_{max} / h) = (0.2, 0.4, 0.6)$  on the dimensionless mean ( $T_{crnl}$ ) and coefficient of variations ( $\lambda_{crnl}$ ) of thermal post buckling load of 4-layers anti-symmetric cross-ply [0/90]2s square plate with simply supported ssss (s2) condition for  $cov, \{b_i, i = (1, \dots, 8), (7, 8) \text{ and } (9) = 0.10\}$  under combination of uniform and transverse temperature (t.t), uniform temperature (u.t) distribution, with simple support ssss (s2) boundary conditions.  $cr1$  – dimensionless linear mean thermal buckling load

a/h	$W_{max} / h$	(TD), T.T			(TD), U.T				
		Mean, $T_{crnl}$	COV, $\lambda_{crnl}$			Mean, $T_{crnl}$	COV, $\lambda_{crnl}$		
			bi				bi		
			(i=1, ..., 8)	i=7,8	(i=9)		(i=1, ..., 8)	i=7,8	(i=9)
30	0.2	0.441	0.2153	0.1462	0.1855	0.441	0.2156	0.1462	0.1855
	0.4	0.5399	0.1753	0.1194	0.1765	0.5399	0.176	0.1194	0.1765
	0.6	0.6516	0.145	0.099	0.1706	0.6516	0.146	0.099	0.1706
	$T_{cr1}$	-0.4003				-0.4003			
40	0.2	0.2536	0.3519	0.2542	0.1856	0.2536	0.3523	0.2542	0.1856
	0.4	0.3121	0.2843	0.2066	0.1752	0.3121	0.2855	0.2066	0.1752
	0.6	0.3886	0.2266	0.1659	0.1678	0.3886	0.2283	0.1659	0.1676
	$T_{cr1}$	-0.2303				-0.2303			

**Table 4** Effects of plate thickness ratios ( $a/h$ ) with foundation parameters on the dimensionless mean and the dispersion of thermal buckling temperature for angle-ply anti-symmetric [450/-450] laminated composite square plate resting on elastic foundation subjected to non-uniform tent-like temperature distribution for  $cov, \{b_i, i = (1, \dots, 8), (7, 8), (9, 10) \text{ and } (11) = 0.10\}$  with ssss boundary conditions

a/h	Foundation parameters	Mean, $T_{crnl}$	COV, $\lambda_{crnl}$			
			bi			
			i=1, ..., 8	i=7, 8	i=9, 10	i=11
5	$(k_1 = 0, k_2 = 0)$	49.5857	0.0996	4.13E-04	0	0.0414
	$(k_1 = 100, k_2 = 0)$	112.851	0.0763	1.80E-04	0.0296	0.0494
	$(k_1 = 100, k_2 = 10)$	278.6206	0.0308	7.28E-05	0.0607	0.1837
10	$(k_1 = 0, k_2 = 0)$	15.4511	0.1022	0.0013	0	0.0318
	$(k_1 = 100, k_2 = 0)$	36.4957	0.0442	5.61E-04	0.0574	0.1514
	$(k_1 = 100, k_2 = 10)$	78.2641	0.0206	2.61E-04	0.0597	0.224
20	$(k_1 = 0, k_2 = 0)$	4.1756	0.1028	0.0049	0	0.0261
	$(k_1 = 100, k_2 = 0)$	9.4379	0.0462	0.0022	0.0556	0.1517
	$(k_1 = 100, k_2 = 10)$	19.8818	0.0219	0.001	0.0588	0.2263

**Figure 5:** Effects of number of layers, aspect ratios ( $a/b$ ), amplitude ratios ( $W_{max}/h$ ) and random input variables [ $b_i$ , ( $i = 1$  to  $8$ ), ( $7, 8$ ) and ( $9$ ) =  $0.10$ ] on dimensionless mean ( $T_{crnl}$ ) and coefficient of variations ( $\lambda_{crnl}$ ) of thermal post buckling load of symmetric cross-ply  $[00/900/00]$  and ant-symmetric  $[00/900]_{2T}$  laminated composite plates under combination of uniform and transverse temperature(t,t), uniform temperature (u.t) distribution., plate thickness ratio ( $a/h=100$ ), with simple support ssss (s2) boundary conditions

No. of layers	a/b	$W_{max}/h$	(TD), T.T			(TD), U.T				
			Mean, $T_{crnl}$	COV, $\lambda_{crnl}$			Mean, $T_{crnl}$	COV, $\lambda_{crnl}$		
				bi				bi		
				(i=1,...,8)	(i=7,8)	(i=9)		(i=1,...,8)	(i=7,8)	(i=9)
[00/900/00]	1	0.2	0.0478	1.911	1.2972	0.1859	0.0478	1.9113	1.2972	0.1859
		0.4	0.0531	1.6958	1.1077	0.234	0.0531	1.6965	1.1077	0.234
		0.6	0.0551	1.6901	1.1684	0.1423	0.0551	1.6912	1.1684	0.1423
	$T_{cr}$	0.0446					-0.0446			
	2	0.2	0.0136	6.4749	4.1785	0.2436	0.0136	6.476	4.1785	0.2436
0.4		0.0196	4.485	2.8901	0.2313	0.0196	4.4872	2.8901	0.2313	
0.6		0.0199	4.4345	2.8642	0.2116	0.0199	4.4372	2.8642	0.2116	
$T_{cr}$		-0.0111					-0.0111			
[00/900] <sub>2T</sub>	1	0.2	0.0423	2.2174	1.5254	0.1852	0.0423	2.218	1.5254	0.1852
		0.4	0.0516	1.8138	1.2495	0.1731	0.0516	1.8154	1.2495	0.1731
		0.6	0.0636	1.4682	1.0133	0.1629	0.0636	1.4706	1.0133	0.1629
	$T_{cr}$	-0.0383					-0.0383			
	2	0.2	0.0333	2.7309	1.8726	0.2318	0.0344	2.7315	1.8726	0.2318
0.4		0.0408	2.2275	1.5597	0.2124	0.0413	2.2731	1.5597	0.2124	
0.6		0.0465	1.9735	1.3575	0.1922	0.0475	1.9743	1.3585	0.1926	
$T_{cr}$		-0.03					-0.0311			

**Figure 6** Effects of aspect ratios ( $a/b$ ), number of layers with random input variables [ $b_i$ , ( $i = 1$  to  $8$ ), ( $7, 8$ ) and ( $9$ ) =  $0.10$ ] on dimensionless mean ( $T_{crnl}$ ) and coefficient of variations ( $\lambda_{crnl}$ ) of thermal post buckling load of laminated composite plates under combination of uniform and transverse temperature(t,t), uniform temperature (u.t) distribution., plate thickness ratio ( $a/h=100$ ), with simple support ssss (s2) boundary conditions

a/b	Lamination scheme	Foundation parameters	Mean, $T_{crnl}$	COV, $\lambda_{crnl}$			
				bi			
				i=1,..., 8	i=7, 8	i=9, 10	i=11
1		$(k_1 = 0, k_2 = 0)$	0.1739	0.1554	0.1177	0	0.0213
	$[45^0 / -45^0]$	$(k_1 = 100, k_2 = 0)$	0.3843	0.0707	0.0533	0.0547	0.1534
		$(k_1 = 100, k_2 = 10)$	0.8021	0.0339	0.0255	0.0583	0.2291
		$(k_1 = 0, k_2 = 0)$	0.1847	0.1446	0.1081	0	0.0369
	$[45^0 / -45^0 / 45^0]$	$(k_1 = 100, k_2 = 0)$	0.3935	0.0689	0.0504	0.0527	0.1389
		$(k_1 = 100, k_2 = 10)$	0.8213	0.0325	0.0243	0.0579	0.2234

Table Continued..

a/b	Lamination scheme	Foundation parameters	Mean, $T_{crnl}$	COV, $\lambda_{crnl}$				
				bi				
				i=1,...,8	i=7,8	i=9,10	i=11	
2	$[45^0 / -45^0]$	$(k_1 = 0, k_2 = 0)$	0.2052	0.1358	0.0992	0	0.0193	
		$(k_1 = 100, k_2 = 0)$	0.2472	0.1128	0.0823	0.017	0.0348	
		$(k_1 = 100, k_2 = 10)$	0.4561	0.0612	0.0446	0.0467	0.156	
		$(k_1 = 0, k_2 = 0)$	0.2197	0.1256	0.091	0	0.0317	
		$[45^0 / -45^0 / 45^0]$	$(k_1 = 100, k_2 = 0)$	0.2616	0.1055	0.0764	0.016	0.0212
		$(k_1 = 100, k_2 = 10)$	0.4736	0.0582	0.0423	0.0456	0.1459	

Figure 7 Effects of boundary conditions(bcs) , amplitude ratios ( $W_{max} / h$ ) and random input variables [bi, (i=1 to 8), (7, 8) and (9) = 0.10] on dimensionless mean ( $T_{crnl}$ ) and coefficient of variations ( $\lambda_{crnl}$ ) of thermal post buckling load of angle-ply antisymmetric [450/-450]2t square laminated composite plates under combination of uniform and transverse temperature(t,t), uniform temperature (u.t) distribution., plate thickness ratio (a/h=50)

BCs	$W_{max} / h$	(TD), T.T				(TD), U.T			
		Mean, $T_{crnl}$	COV, $\lambda_{crnl}$			Mean, $T_{crnl}$	COV, $\lambda_{crnl}$		
			bi	(i=1,...,8)	(i=7,8)		(i= 9)	bi	(i=1,...,8)
SSSS (S1)	0.2	0.2989	0.2813	0.2156	0.1801	0.299	0.2815	0.2157	0.1791
	0.4	0.3277	0.2557	0.1967	0.1736	0.3277	0.2563	0.1967	0.1726
	0.6	0.3706	0.2249	0.1739	0.1658	0.3707	0.2259	0.174	0.1648
	$T_{crl}$	-0.2883				-0.2884			
SSSS	0.2	0.2956	0.2861	0.218	0.1821	0.2957	0.2863	0.2181	0.1809
	0.4	0.324	0.2602	0.1989	0.1752	0.324	0.2608	0.199	0.1741
	0.6	0.3665	0.2291	0.1759	0.1668	0.3665	0.23	0.1759	0.1657
	$T_{crl}$	-0.2851				-0.2851			
CCCC(1)	0.2	0.5721	0.1741	0.1126	0.1919	0.5724	0.1742	0.1127	0.1906
	0.4	0.6249	0.159	0.1031	0.1879	0.625	0.1593	0.1032	0.1866
	0.6	0.7023	0.1409	0.0917	0.1834	0.7023	0.1414	0.0918	0.1822
	$T_{crl}$	-0.5531				-0.5533			
CSCS(2)	0.2	0.408	0.2165	0.158	0.1976	0.4079	0.2167	0.1581	0.1962
	0.4	0.4594	0.1921	0.1404	0.1885	0.4594	0.1925	0.1404	0.1871
	0.6	0.5329	0.165	0.121	0.1796	0.5328	0.1658	0.121	0.1783
	$T_{crl}$	0.3896)				-0.3895			

**Figure 8** Effects of three different support conditions, ssss, cccc and cscs with various foundation parameters) and random input variables [ $b_i$ , ( $i = 1$  to 8), (7, 8) and (9, 10) and (11) = 0.10] on dimensionless mean ( $T_{crnl}$ ) and coefficient of variations ( $\lambda_{crnl}$ ) of thermal post buckling load of cross-ply symmetric [00/900/900/00] laminated composite plates under combination of uniform and transverse temperature (t.t), uniform temperature (u.t) distribution., plate thickness ratio ( $a/h=10$ )

BCs	Foundation parameters	Mean, $T_{crnl}$	COV, $\lambda_{crnl}$			
			bi			
			i=1,..., 8	i=7, 8	i=9, 10	i=11
SSSS	$(k_1 = 0, k_2 = 0)$	14.1382	0.0719	0.0014	0	0.0461
	$(k_1 = 100, k_2 = 0)$	33.0055	0.0935	6.16E-04	0.0255	0.021
	$(k_1 = 100, k_2 = 10)$	74.7823	0.0413	2.72E-04	0.057	0.17
CCCC	$(k_1 = 0, k_2 = 0)$	37.3257	0.0794	5.48E-04	0	0.0475
	$(k_1 = 100, k_2 = 0)$	51.7059	0.1284	3.93E-04	0.0124	0.0227
	$(k_1 = 100, k_2 = 10)$	93.4827	0.071	2.18E-04	0.0452	0.1161
CSCS	$(k_1 = 0, k_2 = 0)$	23.1902	0.0742	8.82E-04	0	0.0464
	$(k_1 = 100, k_2 = 0)$	38.1211	0.0721	5.35E-04	0.0296	0.0429
	$(k_1 = 100, k_2 = 10)$	79.8979	0.0344	2.55E-04	0.0542	0.171

**Figure 9** Effects of temperature change ( $\delta t$ ), amplitude ratios and random input variables [ $b_i$ , ( $i = 1$  to 8), (7, 8) and (9) = 0.10] on dimensionless mean ( $\lambda_{crnl}$ ) and coefficient of variations ( $\lambda_{crnl}$ ) of thermal post buckling load of angle-ply [ $\pm 45$ ] $2t$  square laminated composite plates under combination of uniform and transverse temperature (t.t), uniform temperature (u.t) distribution., plate thickness ratio ( $a/h=20$ )

		(TID)			
$(\Delta T)$	$W_{max} / h$	Mean, $T_{crnl}$	COV, $\lambda_{crnl}$		
			bi		
			(i=1,...,8)	(i=7,8)	(i= 9)
50	0.2	0.0459	0.0733	0.0016	0.0755
	0.4	0.051	0.0677	0.0015	0.0718
	0.6	0.0524	0.0662	0.0014	0.0679
	$T_{crit}$	-0.0439			
100	0.2	0.0229	0.0717	0.0033	0.0755
	0.4	0.0255	0.0663	0.0029	0.0718
	0.6	0.0287	0.0615	0.0026	0.0679
	$T_{crit}$	-0.0219			
150	0.2	0.0153	0.0702	0.0049	0.0755
	0.4	0.017	0.0649	0.0044	0.0718
	0.6	0.0191	0.0602	0.0039	0.0679
	$T_{crit}$	-0.0146			

Table Continued...

		(TID)			
( $\Delta T$ )	$W_{max} / h$	Mean, $T_{crnl}$	$COV, \lambda_{crnl}$		
			bi		
			(i=1,...,8)	(i=7,8)	(i= 9)
200	0.2	0.0115	0.0687	0.0065	0.0755
	0.4	0.0127	0.0636	0.0059	0.0718
	0.6	0.0143	0.0591	0.0052	0.0679
	$T_{crl}$	-0.011			

**Figure 10** Effects of temperature change ( $\delta t$ ), amplitude ratios and random input variables [ $b_i$  ( $i=1$  to 8), (7, 8) and (9) = 0.10] on dimensionless mean ( $T_{crnl}$ ) and coefficient of variations ( $\lambda_{crnl}$ ) of thermal post buckling load of angle-ply [ $\pm 45$ ]<sub>2t</sub> square laminated composite plates under combination of uniform and transverse temperature(t.t), uniform temperature (u.t) distribution., plate thickness ratio ( $a/h=20$ )

		(TD)			
( $\Delta T$ )	$W_{max} / h$	Mean, $T_{crnl}$	$COV, \lambda_{crnl}$		
			bi		
			(i=1,...,8)	(i=7,8)	(i= 9)
50	0.2	0.0306	0.0884	0.0022	0.077
	0.4	0.034	0.0823	0.002	0.072
	0.6	0.0386	0.0785	0.0017	0.067
	$T_{crl}$	-0.0294			
100	0.2	0.0153	0.0861	0.0044	0.077
	0.4	0.017	0.0802	0.004	0.072
	0.6	0.0193	0.0767	0.0035	0.067
	$T_{crl}$	-0.0147			
150	0.2	0.0102	0.0838	0.0066	0.077
	0.4	0.0113	0.0782	0.0059	0.072
	0.6	0.0129	0.0749	0.0052	0.067
	$T_{crl}$	-0.0098			
200	0.2	0.0077	0.0817	0.0088	0.077
	0.4	0.0085	0.0763	0.0079	0.072
	0.6	0.0097	0.0731	0.007	0.067
	$T_{crl}$	-0.0073			

**Table 11** Effects of lamination scheme with foundation parameters and random input variables [bi, (i =1 to 8), (7, 8) and (9) = 0.10] on dimensionless mean ( $T_{crnl}$ ) and coefficient of variations ( $\lambda_{crnl}$ ) of thermal post buckling load of laminated composite plates under combination of uniform and transverse temperature (t.t), uniform temperature (u.t) distribution., plate thickness ratio (a/h=50)

Lamination scheme	Foundation parameters	Mean, $T_{crnl}$	COV, $\lambda_{crnl}$			
			bi			
			i=1,..., 8	i=7, 8	i=9, 10	i=11
[0/90]2T	$(k_1 = 0, k_2 = 0)$	0.3265	0.1026	0.0689	0	0.0419
	$(k_1 = 100, k_2 = 0)$	0.7915	0.0423	0.0284	0.0587	0.1574
	$(k_1 = 100, k_2 = 10)$	1.7098	0.0196	0.1457	0.0602	0.2325
[0/90]2s	$(k_1 = 0, k_2 = 0)$	0.3473	0.0978	0.0648	0	0.0379
	$(k_1 = 100, k_2 = 0)$	0.8123	0.0418	0.0277	0.0572	0.154
	$(k_1 = 100, k_2 = 10)$	1.7306	0.0196	0.013	0.0595	0.23

**Table 12** Effects of material properties, amplitude ratios ( $W_{max} / h$ ) and random input variables [bi, (i =1 to 8), (7, 8) and (9) = 0.10] on dimensionless mean ( $T_{crnl}$ ) and coefficient of variations ( $\lambda_{crnl}$ ) of thermal post buckling load of of angle-ply symmetric [45/-45]2t square laminated composite plates under combination of uniform and transverse temperature (t.t), uniform temperature (u.t) distribution., plate thickness ratio (a/h=100)

Uni-axial compression					
Material properties	$W_{max} / h$	Mean, $T_{crnl}$	COV, $\lambda_{crnl}$		
			bi		
			(i=1,...,8)	(i=7, 8)	(i=9)
TD	0.2	0.1316	1.4007	0.9774	0.3417
	0.4	0.1487	1.2385	0.8655	0.3226
	0.6	0.1676	0.9928	0.6984	0.2833
	$T_{crl}$	-0.1254			
TID	0.2	0.2024	0.9505	0.6977	0.351
	0.4	0.2293	0.8378	0.6161	0.3307
	0.6	0.2533	0.6754	0.5027	0.2909
	$T_{crl}$	-0.1925			



**Figure 13** Effects of material properties, amplitude ratios ( $W_{max} / h$ ) and random input variables [ $b_i$ , ( $i = 1$  to 8), (7, 8) and (9) = 0.10] on dimensionless mean ( $T_{crnl}$ ) and coefficient of variations ( $\lambda_{crnl}$ ) of thermal post buckling load of of angle-ply symmetric [45/-45]2t square laminated composite plates under combination of uniform and transverse temperature (t.t), uniform temperature (u.t) distribution., plate thickness ratio ( $a/h=100$ )

Material properties		$W_{max} / h$	Bi-axial compression			
			Mean, $T_{crnl}$	$COV, \lambda_{crnl}$		
				bi		
				(i=1,...,8)	(i=7, 8)	(i=9)
TD	0.2	0.0659	1.4024	0.9786	0.2422	
	0.4	0.0745	1.2386	0.8656	0.2228	
	0.6	0.0871	1.0565	0.74	0.2023	
	$T_{crl}$	-0.0628				
TID	0.2	0.1014	0.952	0.6987	0.2515	
	0.4	0.1149	0.8379	0.6161	0.2307	
	0.6	0.1347	0.7129	0.5258	0.2092	
	$T_{crl}$	-0.0964				

**Figure 14** The Effect of thermal load ratio  $t_0/t_1$  ( $= 0.0, 0.5, 1.0$ ) with amplitude ratios  $w_{max}/h$  ( $= 0.2, 0.4, 0.6$ ) and random input variables [ $b_i$ , ( $i = 1$  to 8), (7, 8) and (9) = 0.10] on the dimensionless mean ( $T_{crnl}$ ) and dispersion( $\lambda_{crnl}$ ) of thermal post buckling load of 4-layers anti-symmetric angle-ply [450/-450]2t square plate with simply supported ssss (s2) condition and  $a/h=20$  under non-uniform tent like and parabolic temperature distribution

$T_0 / T_1$		$W_{max} / h$	Tent-like			Parabolic				
			$COV, \lambda_{crnl}$			$COV, \lambda_{crnl}$				
			Mean, $T_{crnl}$	bi			Mean, $T_{crnl}$	bi		
				i=1,..., 8	i=7, 8	i=9		i=1,..., 8	i=7, 8	i=9
0	0.2	3.8831	0.0796	0.0059	0.0438	2.0885	0.0795	0.00588	0.041	
	0.4	4.2161	0.0747	0.0054	0.0429	2.266	0.0746	0.00538	0.0402	
	0.6	4.5643	0.0705	0.005	0.0424	2.4533	0.0704	0.005	0.0398	
	$T_{crl}$	-3.7319				-2.0076				
0.5	0.2	1.9411	0.0802	0.0118	0.0438	1.114	0.0802	0.0118	0.0412	
	0.4	2.1061	0.0754	0.0109	0.0429	1.2116	0.0752	0.0108	0.0402	
	0.6	2.2802	0.0711	0.01	0.0425	1.3147	0.071	0.01	0.0394	
	$T_{crl}$	-1.8659				-1.0708				
1	0.2	1.294	0.0813	0.0177	0.0438	1.006	0.0813	0.0177	0.0424	
	0.4	1.4041	0.0763	0.0163	0.0429	1.0942	0.0763	0.0163	0.0415	
	0.6	1.519	0.072	0.0151	0.0426	1.1873	0.072	0.0151	0.0406	
	$T_{crl}$	-1.244				-0.9671				

**Table 15** Nomenclature

$A_{ij}, B_{ij}, etc$	Laminate stiffnesses
a, b	Plate length and breadth
h	Thickness of the plate
$E_f, E_m$	Elastic moduli of fiber and matrix, respectively.
$G_f, G_m$	Shear moduli of fiber and matrix, respectively.
$\nu_f, \nu_m$	Poisson's ratio of fiber and matrix, respectively.
$V_f, V_m$	Volume fraction of fiber and matrix, respectively.
$\alpha_f, \alpha_m$	Coefficient of thermal expansion of fiber and matrix, respectively.
bi	Basic random material properties
$E_{11}, E_{22}$	Longitudinal and Transverse elastic moduli
$G_{12}, G_{13}, G_{23}$	Shear moduli
$K_p$	Linear bending stiffness matrix
$K_g$	Thermal geometric stiffness matrix
D	Elastic stiffness matrices
$M_{\alpha\beta}, m_{\alpha\beta}$	Mass and inertia matrices
ne, n	Number of elements, number of layers in the laminated plate
$N_x, N_y, N_{xy}$	In-plane thermal buckling loads
nn	Number of nodes per element
$N_i$	Shape function of ith node
$\bar{C}^p_{ijkl}$	Reduced elastic material constants
$f, \{f\}^{(e)}$	Vector of unknown displacements, displacement vector of eth element
u, v, w	Displacements of a point on the mid plane of plate
$\bar{u}_1, \bar{u}_2, \bar{u}_3,$	Displacement of a point (x, y, z)
$\bar{\sigma}_{ij}, \bar{\epsilon}_{ij}$	Stress vector, Strain vector
$\psi_y, \psi_x$	Rotations of normal to mid plane about the x and y axis respectively
$\theta_x, \theta_y, \theta_k$	Two slopes and angle of fiber orientation wrt x-axis for kth layer
x, y, z	Cartesian coordinates
$\rho, \lambda, Var(.)$	Mass density, eigenvalue, variance

Table Continued..

$\omega, \bar{\omega}$	Fundamental frequency and its dimensionless form
$RV_s$	
$\Delta T, \Delta X,$	Difference in temperatures and moistures
$\alpha_1, \alpha_2, \beta_1, \beta_2$	Thermal expansion and hygroscopic coefficients along x and y direction, respectively.

## Conclusion

A  $C^0$  FEM and direct iterative method in conjunction with FOPT is employed to compute the mean and standard deviation of the thermal post buckling load of the laminated composite plate with thermo-mechanical properties, random change in all input variables, aspect ratios, amplitude ratios and plate thickness. The following conclusion can be drawn from this limited study:

- i. The characteristics of the thermal buckling load of plates are significantly influenced by various support conditions, plate thickness ratios, aspect ratios, number of layers, lamination scheme and foundation parameters. The first order perturbation technique gives acceptable results for the range of dispersion (SD/mean) taken in the study. The characteristics of the thermal post buckling temperature of plates are significantly influenced by various support conditions, plate thickness ratios, aspect ratios and temperature changes. The mean and dispersion of thermal post buckling temperature of laminated composite plates is higher when the plates are subjected to temperature dependent (TD) thermo-material properties.
- ii. The thermal buckling load strongly depends on the foundation parameters and increases with increase the foundation parameters. The clamp supported plates buckle at slightly higher temperature compared to other supports as mean thermal post buckling temperature is higher and COV is lower for clamped support when compared with other types of support conditions. Post buckling is more dominant in plates of (TD) thermo-material properties. The random change in input variables thickness ( $h$ ) has more impact on thermal post buckling temperature scattering compared to individual random changes in material properties and thermal expansion coefficients.

The dispersion in thermal buckling is the greatest with scatter in  $E_{11}$  and  $h$  in the case of the plate supported without foundation,  $k_1$  and  $h$  for Winkler elastic foundation and  $k_2$  and  $h$  for Pasternak elastic foundation respectively. This means that the care should be taken during fabrication process so as to allow less variation in these system properties with various foundation parameters. The sensitivity of thermal post buckling temperature and COV due to variation in temperature dependent thermo-material properties is dependent mainly on thickness ratio, and boundary conditions besides other parameters of the laminate. The COV in the thermal post buckling temperature is most affected with random change in lamina thickness  $h$  and least affected with scatter in  $G_{12}$ . In general the plate is more sensitive to individual random change in  $E_{11}$ ,  $V_{12}$  and  $\alpha_{11}$ . The strict control of these random parameters is therefore required for reliable design if high reliability of laminated composite plate is required

In general, the square plate is more sensitive as compared to rectangular plate. The thermal post buckling temperature for square plate is more compared to rectangular plate. The thermal post buckling

temperature is more prone to SSSS (S2) boundary conditions while it is least for clamped support CCCC boundary conditions.

The plate with all edges clamped support condition is less desirable in comparison with other support conditions from scattering point of view. The impact of randomness in all random system variables is more for thin plate as compared to thick and moderately thick plate.

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## Conflict of interest

Author declares that there is no conflict of interest.

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